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**TRANSIENT ANALYSIS OF HEAT CONDUCTION  
THROUGH A SLAB BY INFINITE SERIES**

**THOMAS N. BERNSTEIN  
ROBERT M. ENGLE, JR.**

**TECHNICAL REPORT AFFDL-TR-68-109**

**DECEMBER 1968**

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**AIR FORCE FLIGHT DYNAMICS LABORATORY  
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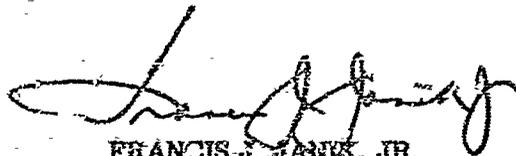
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FOREWORD

This report was prepared by Thomas N. Bernstein and Robert M. Engle, Jr., of the Theoretical Mechanics Branch, Structures Division, Air Force Flight Dynamics Laboratory. The work was conducted in house under Project No. 1467, "Structural Analysis Methods," Task No. 146702, "Thermoelastic Structural Analysis Methods," and was administered by the Air Force Flight Dynamics Laboratory, Research and Technology Division, Air Force Systems Command, Wright-Patterson Air Force Base, Ohio. Mr. Robert M. Bader is the Project Engineer administering Project No. 1467.

This report covers research conducted from July 1964 to July 1966. The manuscript was released by the authors in September 1966 for publication as a technical report.

This technical report has been reviewed and is approved.



FRANCIS S. JANK, JR.  
Chief, Theoretical Mechanics Branch  
Structures Division

ABSTRACT

The exact solution to the problem of conduction of heat through a slab is developed. The solution, formulated in terms of an infinite series, allows arbitrary initial conditions and time-dependent boundary conditions. The solution is programmed in FORTRAN IV for the IBM 7094 II computer. Several check problems were solved and the results were compared with those obtained from a finite difference heat transfer program.

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## SYMBOLS

<u>MATH SYMBOL</u>	<u>FORTRAN SYMBOL</u>	<u>PHYSICAL DEFINITION</u>
$A, A_0, A_L$		Coefficients of Steady State Solution
$B, B_0, B_L$		Coefficients of Steady State Solution
$C_0, C_1, C_2, C_n$		Constants of Integration
$C_p$	CP	Specific heat
D	DETK	Determinant of $K_{ij}$ 's
$F_0, F_L$	FO, FL	boundary condition constants
$f(x), f_x$	FOFX(X)	Initial conditions
K	K	Thermal conductivity
$K_{ij}$	KI1, KI2, . . .	Boundary condition indicators
L	L	Length
n	NTERMS	Summation index
N		Particular value of n
t	T	Time
T	TEMP	Temperature
$T_s, T_s$		Steady state solutions
$T_T, T_T, T_C, T_L$		Transient solutions
$T_{IC}$		Solution of Initial condition problem
T		Complete problem solution
S		Cross-sectional area of slab
x	x	Distance
$X(x)$		Assumed solution

SYMBOLS (Cont'd)

<u>MATH SYMBOL</u>	<u>FORTRAN SYMBOL</u>	<u>PHYSICAL DEFINITION</u>
$\gamma_n$		Repetitive term in solution
$Z, Z_n$	ZN	Eigenvalues
$\infty$		Infinity
$\alpha = k/\rho C_p$	ALPHA	Thermal diffusivity
$\beta, \beta_n$	BETAN	Eigenvalues
$\lambda$	LAMBDA	Dummy time variable
$\pi$	PI	3.1415926
$\rho$	RHO	Density
$\phi_0(t)$	PHIG(T)	Boundary condition time functions
$\phi_L(t)$	PHIL(T)	
$\Phi(t)$		Assumed solution
<u>Subscripts</u>		
IC		Initial condition
L, O		Boundary
P		Pressure
S		Steady state
T		Transient
0, 1, 2, i, j, n, N		Counters

Superscripts

Primes denote differentiation

## SECTION I

### INTRODUCTION

The conduction of heat through a slab is governed by the following partial differential equation.

$$\frac{\partial}{\partial x} \left[ k \frac{\partial T}{\partial x} \right] = \rho c_p \frac{\partial T}{\partial t} \quad (1)$$

For constant thermal diffusivity, this equation simplifies to

$$\frac{\partial^2 T}{\partial x^2} = \frac{1}{\alpha} \frac{\partial T}{\partial t} \quad (2)$$

The exact solution to this equation can be formulated in terms of an infinite series. This report develops the exact solution for arbitrary initial conditions and time dependent boundary conditions. The solution has been programmed in FORTRAN for an IBM 7094 computer and the source program listing is contained in Appendix I.

## SECTION II

### MATHEMATICAL FORMULATION

#### A. BOUNDARY CONDITIONS

The general solution of Equation (2) must satisfy arbitrary initial and time dependent boundary conditions which can be expressed in the following form:

$$T(x, t) = f(x) \quad t = 0 \quad (3)$$

$$K_{11} \frac{\partial T}{\partial x} + K_{12} T = F_0 \phi_0(\lambda) \quad x = 0 \quad (4)$$

$$K_{21} \frac{\partial T}{\partial x} + K_{22} T = F_L \phi_L(\lambda) \quad x = L \quad (5)$$

where the  $K_{ij}$ 's are constants. Selecting different values of these coefficients dictates the mode of heat transfer present at the boundary. By various combinations of constants, the imposition of surface temperature, convection, heat flux or insulation is possible. A more detailed discussion on the interpretation of boundary conditions is contained in Section III, "Applications."

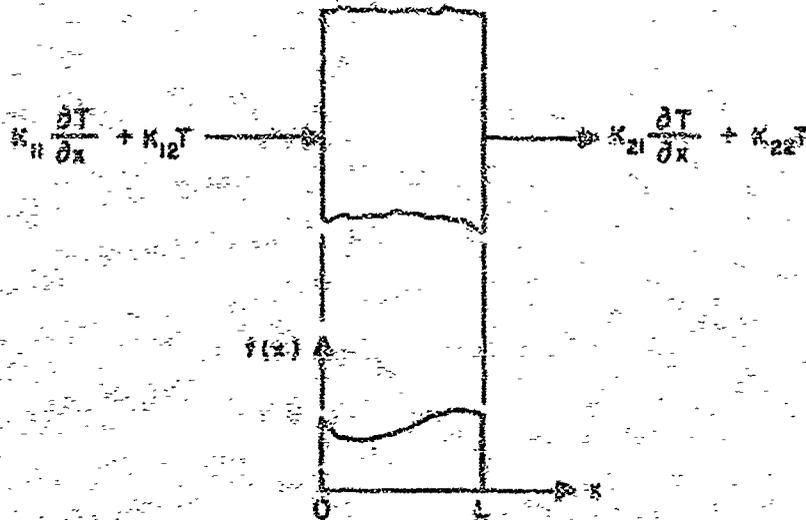


Figure 1. Geometrical Representation

The application of Duhamel's superposition theorem to account for the time dependent boundary conditions necessitated breaking the solution into a transient portion satisfying initial conditions, and a steady state plus transient with zero initial conditions.

Since the restriction has been placed on the boundary conditions that the time dependency can be expressed as a product of a time function and one of the standard boundary conditions, it is therefore possible to solve the equations neglecting the time variation and then modify the solution to account for it.

The problem is first simplified by breaking the solution into two parts: a steady state portion,  $T_s(x, \infty)$ , satisfying the arbitrary boundary condition, and a transient portion,  $T_t(x, t)$ , satisfying the initial temperature distribution and homogeneous boundary conditions.

**B. STEADY STATE SOLUTION**

For steady state conditions we note that  $\frac{\partial T}{\partial t} = 0$  and Equation (3) simplifies to

$$\frac{\partial^2 T}{\partial x^2} = 0 \tag{5}$$

The solution of this equation is found directly by integration with the result;

$$T_s = Ax + B \tag{7}$$

We now impose the arbitrary boundary conditions

$$K_{11} \frac{\partial T}{\partial x} + K_{12} T = F_0 \quad x = 0 \tag{8}$$

$$K_{21} \frac{\partial T}{\partial x} + K_{22} T = F_L \quad x = L \quad (9)$$

Substituting Equation (7) into (8) and (9) yields

$$K_{11} A + K_{12} B = F_0 \quad (10)$$

$$K_{21} A + K_{22}(AL + B) = F_L \quad (11)$$

The constants of integration, A and B, can now be evaluated from Equations (10) and (11). In order to keep these expressions in general form, the solution is accomplished by Cramer's rule with the result

$$A = \frac{K_{12} F_L - K_{22} F_0}{K_{12} K_{22} L - (K_{11} K_{22} - K_{12} K_{21})} \quad (12)$$

$$B = \frac{(K_{21} + K_{22} L) F_0 - K_{11} F_L}{K_{12} K_{22} L - (K_{11} K_{22} - K_{12} K_{21})} \quad (13)$$

### C. TRANSIENT SOLUTION

A product form of solution is assumed for Equation (2), and designated by  $X(x)\Phi(t)$ . Substitution into Equation (2) yields

$$X'' \Phi = \frac{1}{a} X \Phi' \quad (14)$$

Rearranging

$$\frac{X''}{X} = \frac{\Phi'}{a\Phi} \quad (15)$$

which requires that each of these functions be equivalent to some, as yet arbitrary constant. Then setting this constant equal to  $-\beta^2$  results in two ordinary differential equations of the form

$$\Phi' + a\beta^2 \Phi = 0 \quad (16)$$

$$X'' + \beta^2 X = 0 \quad (17)$$

Equation (16) has the exponential form of solution

$$\Phi = C_0 e^{-a\beta^2 t} \quad (18)$$

whereas Equation (17) is satisfied by

$$X(x) = C_1 \cos \beta x + C_2 \sin \beta x \quad (19)$$

The solution to Equation (3) is then

$$T(x, t) = [C_1 \cos \beta x + C_2 \sin \beta x] [C_0 e^{-a\beta^2 t}] \quad (20)$$

This transient solution must satisfy the initial temperature distribution and homogeneous boundary conditions as follows:

$$T(x, t) = f(x) \quad t = 0 \quad (3)$$

$$K_{11} \frac{\partial T}{\partial x} + K_{12} T = 0 \quad x = 0 \quad (21)$$

$$K_{21} \frac{\partial T}{\partial x} + K_{22} T = 0 \quad x = L \quad (22)$$

Note first that the constant  $C_0$  can be eliminated since its effect can be included in  $C_1$  and  $C_2$ . To evaluate the remaining constants substitute Equation (20) into Equations (3), (21) and (22).

Substitution of Equation (20) into (21) yields

$$K_{12} C_1 + K_{11} \beta C_2 = 0 \quad (23)$$

from which we obtain

$$C_1 = -\frac{K_{11} \beta}{K_{12}} C_2 \quad (24)$$

At this point it becomes necessary to impose the artificial restriction that  $K_{12} \neq 0$ , in order that calculations performed on the computer remain bounded.

Substitution of Equation (20) into (22) yields

$$[K_{22} \cos \beta L - K_{21} \sin \beta L] C_1 + [K_{21} \beta \cos \beta L + K_{22} \sin \beta L] C_2 = 0 \quad (25)$$

To obtain a nontrivial solution for  $C_1$  and  $C_2$ , the determinant of their coefficients must be set equal to zero. This yields the following transcendental equation.

$$\tan z = \frac{DLz}{K_{21} K_{11} z^2 + K_{22} K_{12} L^2} \quad (26)$$

where

$$z = \beta L \quad (27)$$

and

$$D = K_{11} K_{22} - K_{12} K_{21} \quad (28)$$

Equation (26) has infinitely many solutions (eigenvalues), and we shall denote these by  $Z_n$ , where  $n = 0, 1, 2, \dots$ . The remaining constant  $C_2$  is evaluated by substituting our solution into Equation (3) in order that the initial temperature distribution be satisfied. It is obvious at this point that, in general, arbitrary functions for the initial temperature distribution can not be satisfied using only one value of  $Z_n$  and  $C_2$ . We are thus required to expand our initial condition and our solution in an infinite series. Then the coefficient  $C_2$  becomes  $C_n$  and its evaluation proceeds as follows. The total solution at this point can be expressed

$$T(x,t) = Ax + B + \sum_{n=0}^{\infty} C_n \left[ \sin \beta_n x - \frac{K_{11} \beta_n}{K_{12}} \cos \beta_n x \right] e^{-\alpha \beta_n^2 t} \quad (29)$$

Imposing the problem initial condition yields

$$T(x,0) = f(x) = Ax + B + \sum_{n=0}^{\infty} C_n \left[ \sin \beta_n x - \frac{K_{11} \beta_n}{K_{12}} \cos \beta_n x \right] \quad (30)$$

Rearranging

$$f(x) - (Ax+B) = \sum_{n=0}^{\infty} C_n \left[ \sin \beta_n x - \frac{K_{11} \beta_n}{K_{12}} \cos \beta_n x \right] \quad (31)$$

Since the sines and cosines form a complete set of orthogonal functions, the  $C_n$ 's can be evaluated by multiplying both sides of Equation (31) by

$$\left[ \sin \beta_N x - \frac{K_{11} \beta_N}{K_{12}} \cos \beta_N x \right] \text{ and integrating from zero to } L.$$

Thus,

$$\int_0^L [f(x) - (Ax+B)] \left[ \sin \beta_N x - \frac{K_{11} \beta_N}{K_{12}} \cos \beta_N x \right] dx = \int_0^L \sum_{n=0}^{\infty} C_n \left[ \sin \beta_n x - \frac{K_{11} \beta_n}{K_{12}} \cos \beta_n x \right] \left[ \sin \beta_N x - \frac{K_{11} \beta_N}{K_{12}} \cos \beta_N x \right] dx \quad (32)$$

By orthogonality this integration produces nontrivial results only in the case of  $n = N$ . Therefore

$$C_n = \frac{\int_0^L [f(x) - (Ax+B)] \left[ \sin \beta_n x - \frac{K_{11} \beta_n}{K_{12}} \cos \beta_n x \right] dx}{\int_0^L \left[ \sin \beta_n x - \frac{K_{11} \beta_n}{K_{12}} \cos \beta_n x \right]^2 dx} \quad (33)$$

The denominator of  $C_n$  can be evaluated directly with the result:

$$\int_0^L \left[ \sin \beta_n x - \frac{K_{11} \beta_n}{K_{12}} \cos \beta_n x \right]^2 dx = \frac{1}{2\beta_n} \left\{ z_n \left[ \left( \frac{K_{11} \beta_n}{K_{12}} \right)^2 + 1 \right] \right. \\ \left. + \sin z_n \cos z_n \left[ \left( \frac{K_{11} \beta_n}{K_{12}} \right)^2 - 1 \right] + 2 \left( \frac{K_{11} \beta_n}{K_{12}} \right) \sin^2 z_n \right\} \quad (34)$$

Collecting the formulations required for problem evaluation leads to the expression of the solution for time independent boundary conditions in the form

$$T(x, t) = Ax + B$$

$$+ \sum_{n=0}^{\infty} \frac{\int_0^L [f(x) - (Ax+B)] [Y_n(x)] dx}{\int_0^L [Y_n(x)]^2 dx} [Y_n(x)] e^{-\alpha \beta_n^2 t} \quad (35)$$

where

$$A = \left[ \frac{K_{12} F_L - K_{22} F_0}{K_{11} K_{22} L - D} \right] \quad (36)$$

$$B = \left[ \frac{(K_{21} + K_{22} L) F_0 - K_{11} F_L}{K_{11} K_{22} L - D} \right] \quad (37)$$

$$Y_n(x) = \left[ \sin \beta_n x - \frac{K_{11} \beta_n}{K_{12}} \cos \beta_n x \right] \quad (38)$$

$$\beta_n = z_n / L \quad (39)$$

and

$$\tan z_n = Z_n = \frac{DL Z_{11}}{K_{21} K_{11} Z_n^2 + K_{22} K_{12} L^2} \quad (40)$$

**D. MODIFICATION OF SOLUTION FOR TIME DEPENDENT BOUNDARY CONDITIONS**

Duhamel's superposition integral is now applied to the solution, Equation (35), to account for the time varying boundary conditions. F. B. Hildebrand gives the solution in the form\*

$$\bar{T}(x, t) = T_0(x, \omega) \phi(x) + \left\{ \phi(0) + \int_0^t e^{-\alpha \beta_n^2 \lambda} \dot{\phi}(\lambda) d\lambda \right\} T_0(x) \quad (41)$$

This formulation is based on certain limitations, however, which must be eliminated. The first is the assumption of zero initial conditions. This restriction is eliminated by considering a

\*Hildebrand, F. B., Introduction to Numerical Analysis, McGraw-Hill Book Company, Inc., New York, 1956.

separate problem, possessing the given initial conditions and homogeneous boundary conditions. The solution of this problem is added to Equation (41). The second simplification utilized to obtain Equation (41) was to hold one boundary at zero and consider the remaining boundary to vary with time. For our problem, both boundaries can vary with time so we make use of the superposition principle once again by varying first one boundary condition and then the other, with the remaining boundary held at zero. The two results are then added. Note that  $f(x) = 0$  for both these solutions.

#### E. SOLUTION OF INITIAL CONDITION PROBLEM

For the given initial condition, Equation (3), and the homogeneous boundary conditions, Equations (21) and (22), a "zero" steady state solution is obtained from Equation (7), i.e.,  $A = 0$ ,  $B = 0$ . Employing the given initial condition in Equation (35) then yields the desired result.

$$T_{IC}(x,t) = \sum_{n=1}^{\infty} \frac{\int_0^L f(x) [Y_n(x)] dx}{\int_0^L [Y_n(x)]^2 dx} [Y_n(x)] e^{-\alpha \beta_n^2 t} \quad (42)$$

#### F. UNSTEADY STATE SOLUTION

The steady state solution,  $T_S(x, \infty)$ , employed in Equation (35) is modified to  $T_S(x, \infty) \phi(t)$  in Equation (41). This result can be viewed as the steady state solution to a problem with our boundary conditions, if those conditions were "frozen" at the instant  $t$ , and remained constant as  $t \rightarrow \infty$ . Since our boundary conditions vary continuously with time, it is not possible to reach a steady state condition. This explains the title employed for this section of the report.  $T_S(x, \infty) \phi(t)$  can be obtained immediately from Equation (7), using boundary condition Equations (4) and (5) in place of (3) and (9). The result is

$$T_S \phi(t) = T_0 = Ax + B \quad (43)$$

where

$$A = \frac{K_{12} F_L \phi_L(t) - K_{22} F_0 \phi_0(t)}{K_{12} K_{22} L - D} \quad (44)$$

$$B = \frac{(K_{21} + K_{22} L) F_0 \phi_0(t) - K_{11} F_L \phi_L(t)}{K_{12} K_{22} L - D} \quad (45)$$

#### G. TRANSIENT SOLUTION (TIME VARIABLE BOUNDARY CONDITIONS)

The transient solution for boundary condition Equations (4) and (5) must be evaluated in two parts as indicated in Section II D. First, consider the conditions

$$K_{11} \frac{\partial T}{\partial x} + K_{12} T = F_0 \phi_0(x) \quad (4)$$

and

$$K_{21} \frac{\partial T}{\partial x} + K_{22} T = 0 \quad (22)$$

with

$$f(x) = 0 \quad (46)$$

Equations (44) and (45) for  $A$  and  $B$  are modified by letting  $F_L = 0$ , with the result

$$A_0 = \frac{-K_{22} F_0 \phi_0(t)}{K_{12} K_{22} L - D} \quad (47)$$

$$B_0 = \frac{(K_{21} + K_{22} L) F_0 \phi_0(t)}{K_{12} K_{22} L - D} \quad (48)$$

The transient solution is obtained by substituting these results into the transient solution in Equation (35) with the result

$$\mathbb{T}_{T_0} = \sum_{n=0}^{\infty} \frac{\int_0^L (-B_0 - A_0 x) Y_n(x) dx}{\int_0^L [Y_n(x)]^2 dx} [Y_n(x)] e^{-\alpha \beta_n^2 t} \quad (49)$$

Similarly for the conditions

$$K_{11} \frac{\partial T}{\partial x} + K_{12} T = 0 \quad (5)$$

$$K_{21} \frac{\partial T}{\partial x} + K_{22} T = F_L \phi_L(t) \quad (21)$$

$$f(x) = 0 \quad (45)$$

and letting  $F_0 = 0$  in Equations (41) and (45), with the result

$$A_L = \frac{K_{12} F_L \phi_L(t)}{K_{12} K_{22} L - D} \quad (50)$$

$$B_L = \frac{-K_{11} F_L \phi_L(t)}{K_{12} K_{22} L - D} \quad (51)$$

we obtain from Equation (35) the transient solution

$$\mathbb{T}_{T_L} = \sum_{n=0}^{\infty} \frac{\int_0^L (A_L x - B_L) Y_n(x) dx}{\int_0^L [Y_n(x)]^2 dx} [Y_n(x)] e^{-\alpha \beta_n^2 t} \quad (52)$$

## H. COMPLETE SOLUTION FOR THE GENERAL PROBLEM

The general form of the complete solutions was expressed by Equation (41). Collecting the solutions obtained in Equations (42), (43), (49) and (52), and substituting into Equation (41), yields the final result,

$$\begin{aligned} \bar{w}(x,t) = & \bar{w}_0 + \left\{ \phi_0(0) + \int_0^1 e^{-\alpha \beta_n^2 \lambda} \phi_0'(\lambda) d\lambda \right\} \bar{w}_{T_0}(x,t) \\ & + \left\{ \phi_L(0) + \int_0^1 e^{-\alpha \beta_n^2 \lambda} \phi_L'(\lambda) d\lambda \right\} \bar{w}_{T_L}(x,t) + \bar{w}_{IC}(x,t) \end{aligned} \quad (53)$$

### SECTION III APPLICATIONS

The generalized boundary conditions utilized in the mathematical formulation can be specialized to handle a number of physical problems. For example, take Equation (5)

$$K_{21} \frac{\partial T}{\partial x} + K_{22} T = F_L \phi_L(\lambda) \quad (5)$$

Appropriate choices of the indicators lead to the following:

- a. Prescribed constant surface temperature.

Let  $K_{21} = 0$ ,  $K_{22} = 1$ ,  $\phi_L(\lambda) = 1$ ,  $F_L =$  applied temperature

- b. Prescribed constant heat flux.

Let  $K_{21} = KS$ ,  $K_{22} = 0$ ,  $\phi_L(\lambda) = 1$ ,  $F_L =$  applied flux

- c. Insulated boundary.

Let  $K_{21} = KS$ ,  $K_{22} = 0$ ,  $\phi_L(\lambda) = 1$ ,  $F_L = 0$

- d. Linear heat transfer at the surface (convection).

Let  $K_{21} = KS$ ,  $K_{22} = -hS$ ,  $\phi_L(\lambda) = 1$ ,  $F_L = -hST_c$

This results in a boundary condition equation of the form

$$KS \frac{\partial T}{\partial x} = hS (T - T_c)$$

where  $h$  is the usual convective heat transfer coefficient per unit area.

- e. Sign Convention.

The sign convention is such that a positive sign indicates flux into the body.

The boundary conditions described in "a" and "b" above may be arbitrarily varied with time by applying the appropriate time function,  $\phi_L(\lambda)$ .

## SECTION IV

COMPUTER PROGRAM FOR SERIES TRANSIENT  
ANALYSIS OF SLAB HEAT TRANSFER (STASH)

## A. DESCRIPTION

The program described below was written to solve for the temperature distribution in a one-dimensional rod with arbitrary initial conditions and time-varying boundary conditions. STASH is coded in FORTRAN IV for the IBM 7044-7094 II Direct Coupled-System. Fifteen subprograms make up the program, each of which has a specific task to perform. These subprograms are listed below.

- MAIN - reads in data, sets up calculations, and prints the results.
- SOLVE 1 - solves the eigenvalue equation for positive values of DETK (see Appendix II).
- SOLVE 2 - solves the eigenvalue equation for negative values of DETK.
- SOLVE 3 - solves the eigenvalue equation for a zero value of DETK.
- SOLVE 4 - solves the eigenvalue equation for DETK infinite.
- FINT - Simpson's rule integration routine.
- FUNCX - sets up the integrand for the x integral
- FUNCT - sets up the integrand for the  $\lambda$  integral
- TABIN - reads in tabular data, if present
- INTERP - performs linear interpolation on tabular data
- PHIO - defines the time varying boundary condition at  $x = 0$
- PHIL - defines the time varying boundary condition at  $x = L$
- PHIPRO - defines the derivative of the time-varying boundary condition at  $x = 0$
- PHIPRL - defines the derivative of the time-varying boundary condition at  $x = L$
- FOFX - defines the initial conditions in the rod.

Figure 2 is a simplified flow chart depicting the transfer of information between the subprograms discussed above.

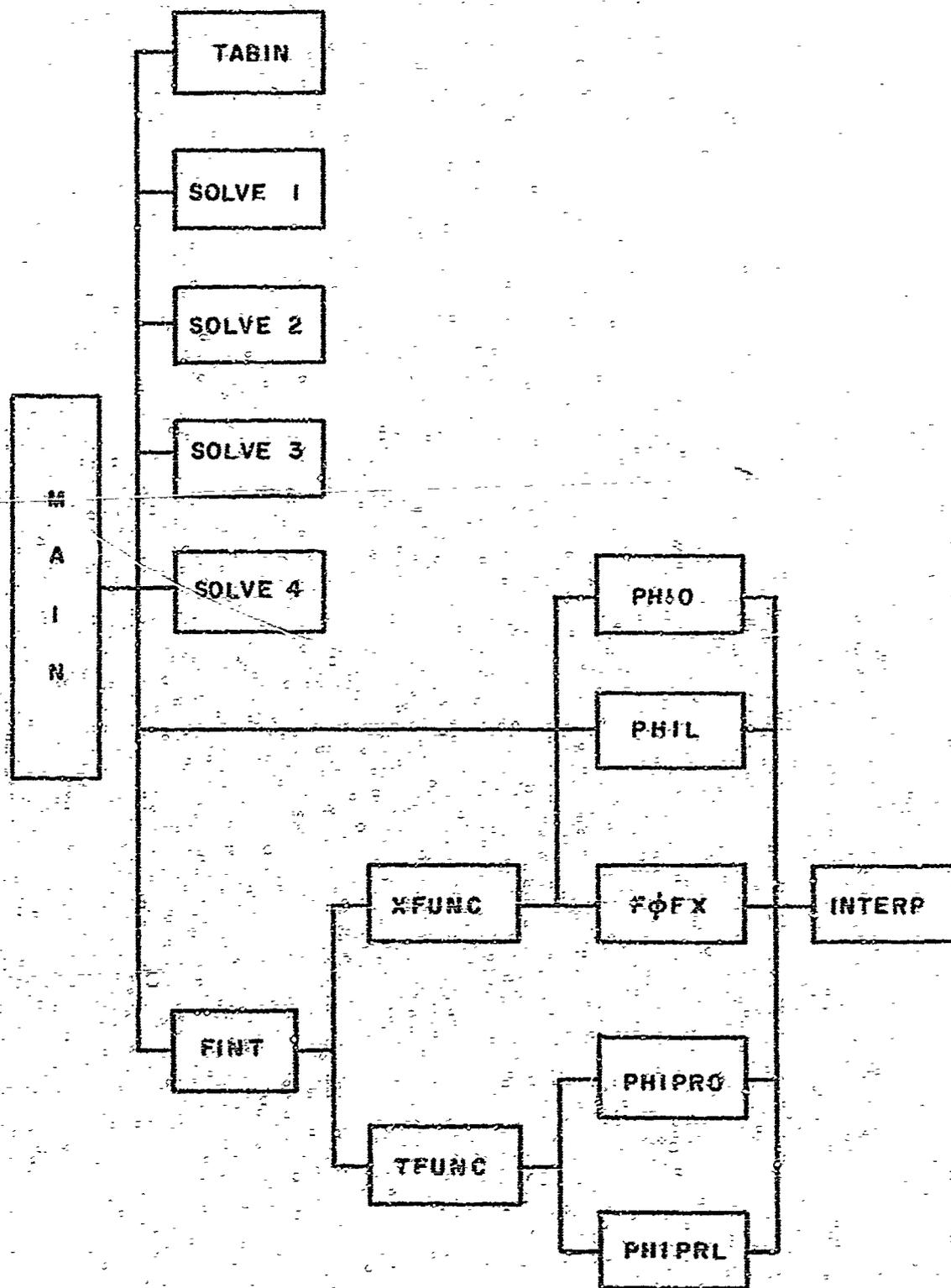


Figure 2. Simplified Flow Chart of Transfer of Information

## B. INPUT

There are basically two types of input data to STASH, the physical parameters and the problem parameters. The physical parameters are the characteristics of the rod and the conditions to which it is subjected. The problem parameters are the accuracy parameters, the calculation controls and the print controls.

The rod is characterized by four basic quantities: length, mass density, thermal conductivity and specific heat. The boundary conditions are identified by the indicators  $K_{11}$ ,  $K_{12}$ ,  $K_{21}$ ,  $K_{22}$ . The magnitude of the boundary conditions is characterized by the indicators  $F_0$  and  $F_L$ . The magnitude of the initial conditions is similarly characterized by the indicator  $F_x$ .

Since the solution may be required at any station on the rod for any given point in time, it is convenient to specify a length increment and a time increment as input parameters. A final time is also specified to terminate calculations. The accuracy of the solution is basically governed by three factors: the accuracy of the eigenvalues, the number of terms in the series portion of the solution and the number of intervals taken in the numerical integration routine. In the interest of maximum flexibility, each of these quantities was made an input parameter.

Information may be input to the program in two basic forms. The first type is the data card. There will always be seven cards in the data deck. If the tabular data option is used there may be many more. The second type of input consists of FORTRAN IV statements which may be inserted into the subprograms defining the initial and boundary conditions on the rod. An example problem using both types of input is given in Section V C. Detailed instructions on inputting the data cards are given below, in the following format:

- (1) Card number and contents
- (2) Program name for contents
- (3) Format of card input referenced to format statement number
- (4) Description of each variable on the card

## 1. Data Cards

Card 1 Intermediate print options

JPRINT(1), JPRINT(2), JPRINT(3)

5000 FORMAT(3I1)

JPRINT(1) - prints series portion of solution term by term if a one is entered. If no print is desired enter a zero.

JPRINT(2) - prints unsteady state portion of the solution if a one is entered. If no print is desired enter a zero.

JPRINT(3) - prints solution for eigenvalues if a one is entered. If no print is desired enter a zero.

Card 2 Title Card

IUNIT, TITLE

1 FORMAT (I2, 13A6)

IUNIT - an indicator which prints out the system of units to be used in the problem. See Table I for a list of systems presently contained in the program.

TITLE - any alphanumeric information through column 80.

Card 3 Physical Parameters (all must be in consistent units)

L, K, RHO, CP, DELTAX, DELTAT, TIMEF

2 FORMAT (7E10.0)

L length of the rod

K thermal conductivity

RHO mass density

CP specific heat

DELTAX increment of length (100 increments maximum)

DELTAT increment of time

TIMEF final time (initial time is zero)

Card 4 Boundary Condition Indicators

K11, K12, K21, K22

3 FORMAT (4E10.0)

K11 indicator for  $\frac{\partial T}{\partial x}$  at  $x = 0$ K12 indicator for T at  $x = 0$ K21 indicator for  $\frac{\partial T}{\partial x}$  at  $x = L$ K22 indicator for T at  $x = L$ Card 5 Function Multiplying Factors

FO, FL, FX

4 FORMAT (3E10.0)

FO coefficient on function  $\phi_0(t)$ FL coefficient on function  $\phi_L(t)$ FX coefficient on function  $f(x)$

TABLE I  
SYSTEMS OF UNITS STORED INTERNALLY

IUNIT	LENGTH	MASS	TIME	WEIGHT	TEMPERATURE
1	INCH	SLUG	SEC	POUND	FAHRENHEIT
2	INCH	SLUG	MIN	POUND	FAHRENHEIT
3	INCH	SLUG	HR	POUND	FAHRENHEIT
4	FOOT	SLUG	SEC	POUND	FAHRENHEIT
5	FOOT	SLUG	MIN	POUND	FAHRENHEIT
6	FOOT	SLUG	HR	POUND	FAHRENHEIT
7	INCH	POUND	SEC	POUND	FAHRENHEIT
8	INCH	POUND	MIN	POUND	FAHRENHEIT
9	INCH	POUND	HR	POUND	FAHRENHEIT
10	FOOT	POUND	SEC	POUND	FAHRENHEIT
11	FOOT	POUND	MIN	POUND	FAHRENHEIT
12	FOOT	POUND	HR	POUND	FAHRENHEIT

Card 6 Calculation Parameters

NTERMS, NSTEPX, NSTEPT, NTAB(1), NTAB(2), NTAB(3), NTAB(4),  
 NTAB(5);

5 FORMAT (SI5, 5H)

- NTERMS - number of terms in the series portion of the solution (100 maximum)
  - NSTEPX - number of intervals for the x-integration
  - NSTEPT - number of intervals for the  $\lambda$ -integration
  - NTAB(1) - flag for table 1
  - NTAB(2) - flag for table 2
  - NTAB(3) - flag for table 3
  - NTAB(4) - flag for table 4
  - NTAB(5) - flag for table 5
- NTAB(I) = 0 Do not use Table  
 NTAB(I) = 1 Use Table

If NSTEPX or NSTEPT is zero the program sets the value of the respective integral to zero.

Card 7 Eigenvalue Solution Parameters

LIMIT, ITERMX

6 FORMAT (E10.0, I5)

- LIMIT - difference between two successive iterations necessary to define convergence to a root.
- ITERMX - maximum number of iterations to be made in searching for each eigenvalue.

If no tabular data is to be used, this is the last card in the data deck. If tabular data is to be an input, however, the following format will be used.

Card 8 Table Number and Comments

NTABLE, COMMENTS

FORMAT (I5, 20x, 53H )

NTABLE table number

COMMENTS any alphanumeric information in columns 20 through 80.

Card 2 Tabular Data ((2 to 50 data cards per table)

INDVAR, DEPVAR, COMMENTS

FORMAT (5X, 2E10.0, 55H )

INDVAR independent variable

DEPVAR dependent variable

COMMENTS any alphanumeric information in columns 26 through 80

Card 3 End of Table

N

FCRMT (15)

N negative of table number

There are five tables provided in the program, which are assigned as follows:

Table 1 PHIQ

Table 2 PHIL

Table 3 PHIPRO

Table 4 PHIPRL

Table 5 EOPX

Figure 3. shows a symbolic data deck. A sample problem is generated in detail in Section IV C.

## 2. Subprogram Input Cards

If the tabular data option is not used STAS<sup>u</sup> calculates the required functions internally using FORTRAN statements as loaded in the subprograms at compilation time. The affected subprograms are:

FUNCTION PHIQ

FUNCTION PHIL

FUNCTION PHIPRO

FUNCTION PHIPRL

FUNCTION EOPX

As the initial or boundary conditions change, cards containing the functional statement of the variation must be inserted. Since all the above functions have an associated multiplying factor

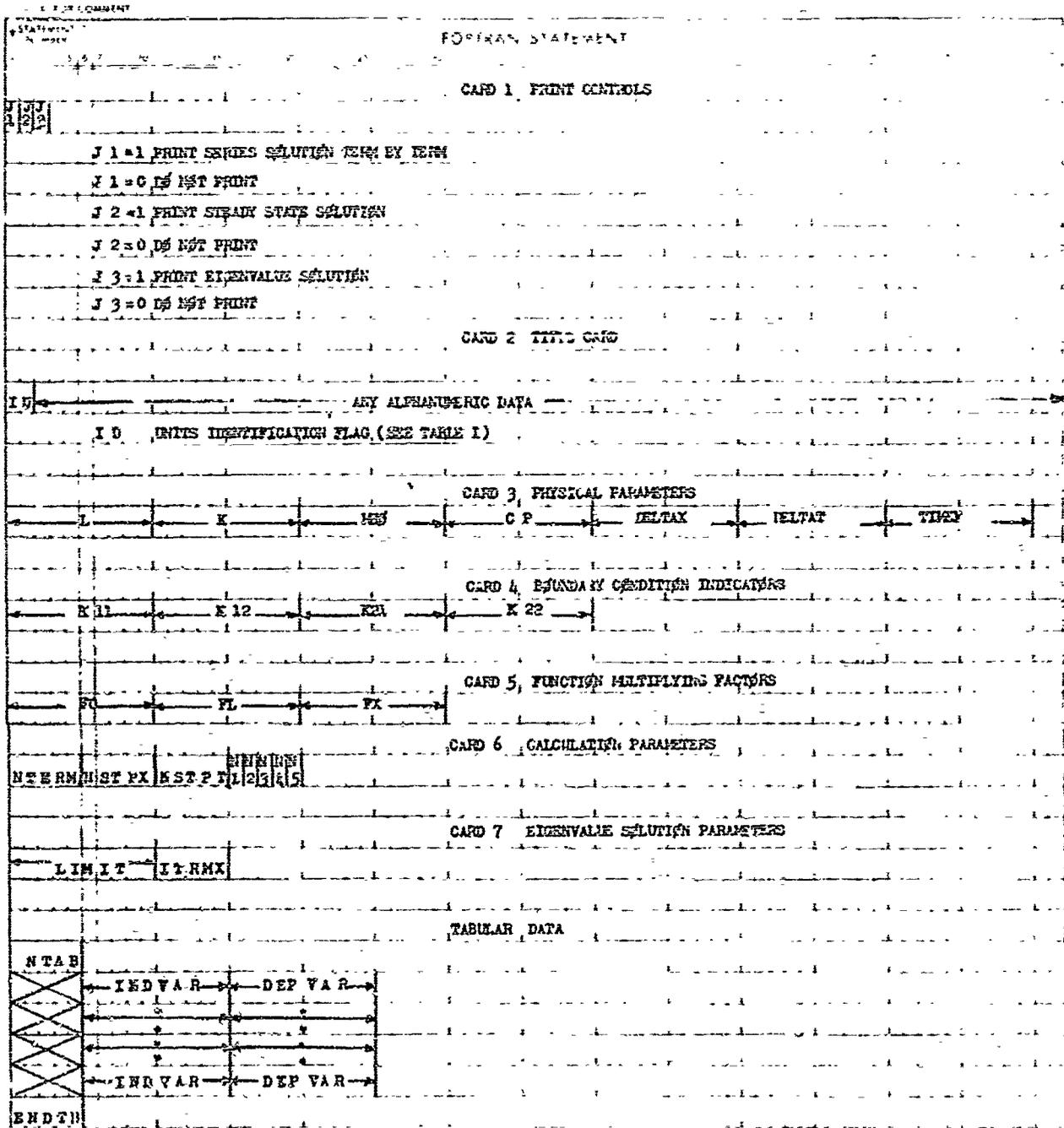


Figure 3. Input Data Format

it is convenient to use normalized functional statements in the subprogram. Thus, if we entered the following card in the FUNCTION FOFX

$$\text{FOFX} = 1.0$$

we would obtain the initial condition

$$f(x) = FX$$

The program (Appendix I) contains subprogram statements corresponding to the following initial and boundary conditions.

$$\phi_0(t) = \text{const}$$

$$\phi_L(t) = \text{const}$$

$$\phi'_0(t) = 0$$

$$\phi'_L(t) = 0$$

$$f(x) = \text{const}$$

### C. SAMPLE PROBLEM

Consider a rod, ten inches long, having the following properties:

$$K = 10 \text{ Btu/hr-ft-}^\circ\text{F}$$

$$\rho = 500 \text{ lb}_m/\text{ft}^3$$

$$c_p = 0.1 \text{ Btu/lb}_m$$

We wish to obtain a time history of the temperature - distribution through the rod which is subject to the following boundary conditions

$$T(0, t) = t$$

$$T(L, t) = 0$$

The initial conditions imposed on the rod are:

$$T(x, 0) = 0$$

For purposes of illustration the intermediate print option will be called out on card one.

The first task in setting up the problem is to decide upon a system of units to employ. Since the length of the rod is given in inches, we shall choose the inch as the unit of length. For a transient study a small time unit is desirable, hence, the second becomes the unit of time. The remainder of the system of units is determined by the temperature and mass units. Going now to Table I, we obtain the correct value of IUNIT. This indicator along with a suitable title becomes card two in Figure 4.

FORTRAN CODING FORM

C FOR COMMENT		STMT NO	5	6	7	10	15	20	25	30	35	40	45	50	55	60	65	70	75
1		1.1.1																	
2		1.0.0				SAMPLE PROBLEM INPUT DATA													
3		0.0.0				0.0	0.2	3.1	4.0	0.28	9.15								
4		1.0.0				1.0				0.0						0.5	0.1		
5		1.0.0				0.0				0.0									
6		2.5.0				5.0				1.0	10.0								
7		0.5.0				20.0													
8		1.0.0																	
9		1.0.00																	
10		1.0.00																	
11		1.0.00																	
12		1.0.00																	
13		1.0.00																	
14		1.0.00																	
15		1.0.00																	
16		1.0.00																	
17		1.0.00																	
18		1.0.00																	
19		1.0.00																	
20		1.0.00																	
21		1.0.00																	
22		1.0.00																	
23		1.0.00																	
24		1.0.00																	
25		1.0.00																	
26		1.0.00																	
27		1.0.00																	
28		1.0.00																	
29		1.0.00																	
30		1.0.00																	
31		1.0.00																	
32		1.0.00																	
33		1.0.00																	
34		1.0.00																	
35		1.0.00																	
36		1.0.00																	
37		1.0.00																	
38		1.0.00																	
39		1.0.00																	
40		1.0.00																	
41		1.0.00																	
42		1.0.00																	
43		1.0.00																	
44		1.0.00																	
45		1.0.00																	
46		1.0.00																	
47		1.0.00																	
48		1.0.00																	
49		1.0.00																	
50		1.0.00																	
51		1.0.00																	
52		1.0.00																	
53		1.0.00																	
54		1.0.00																	
55		1.0.00																	
56		1.0.00																	
57		1.0.00																	
58		1.0.00																	
59		1.0.00																	
60		1.0.00																	
61		1.0.00																	
62		1.0.00																	
63		1.0.00																	
64		1.0.00																	
65		1.0.00																	
66		1.0.00																	
67		1.0.00																	
68		1.0.00																	
69		1.0.00																	
70		1.0.00																	
71		1.0.00																	
72		1.0.00																	
73		1.0.00																	
74		1.0.00																	
75		1.0.00																	
76		1.0.00																	
77		1.0.00																	
78		1.0.00																	
79		1.0.00																	
80		1.0.00																	
81		1.0.00																	
82		1.0.00																	
83		1.0.00																	
84		1.0.00																	
85		1.0.00																	
86		1.0.00																	
87		1.0.00																	
88		1.0.00																	
89		1.0.00																	
90		1.0.00																	
91		1.0.00																	
92		1.0.00																	
93		1.0.00																	
94		1.0.00																	
95		1.0.00																	
96		1.0.00																	
97		1.0.00																	
98		1.0.00																	
99		1.0.00																	
100		1.0.00																	

Figure 4. Sample Problem Data Deck

Card three contains the physical parameters of the system in the system of units called for by the indicator, IUNIT. These parameters are:

$$L = 10 \text{ in.} \quad K = 0.002314 \text{ Btu/in.-sec-}^\circ\text{F} \quad \text{RHO} = 0.2895 \text{ lb}_m/\text{in.}^3$$

$$\text{CP} = 0.10 \text{ Btu/lb}_m \quad \text{DELTAX} = 0.5 \text{ in.} \quad \text{DELTAT} = 100 \text{ sec} \quad \text{TIME} = 1000 \text{ sec}$$

Since we have only temperature boundary conditions we set  $K_{11} = K_{21} = 0$  and  $K_{12} = K_{22} = 1$ . This information is entered on card four.

The functions defining our initial conditions are

$$\phi_0(t) = t, \quad \phi_L(t) = 0, \quad f(x) = 0, \quad \phi_0'(\lambda) = 1, \quad \phi_L'(\lambda) = 0$$

We can take advantage of the functions already stored in the program by using  $F_L$  and  $F_x$  to zero out the appropriate functions. We then can use  $F_0 = 1$  to bring in the other boundary condition. This is shown on card five.

The calculation parameters are entered on card six. A series solution containing twenty-five terms is completely adequate for this problem. Since the initial condition function is zero, we set NSTEPX equal to zero. For a Simpson's rule integration scheme fifty steps should suffice for NSTEPT. Our choice of multiplying factors on card five enabled us to do much of the function calculation internally. However, to eliminate recompiling any portion of the program we used tables to define the functions  $\phi_0(t)$  and  $\phi_0'(\lambda)$ . Thus we set NTAB(1) and NTAB(3) equal to one and the rest equal to zero.

For a solution with temperature boundaries only, the eigenvalues become simply  $n\pi$ . Thus, the eigenvalue parameters have little meaning. However, for a more complex case they would have a significant effect on the solution so these parameters should be made as stringent as required. Typical values are entered on card seven.

Our choice not to recompile any subprograms leads to the use of tables one and three. The first card in each table is a table designation number. The following cards contain data points. The last card of each table contains the negative of the table designation number and is a flag signalling the end of the table.

This, then is the data deck for the sample problem. The assembled deck is shown in Figure 4.

#### D. RESTRICTIONS

Certain restrictions must be adhered to in order for the solution to be successful. Violation of these restrictions will usually produce an error message from the computer program.

a. A consistent set of units must be employed. An indicator is provided on the title card which will label the system of units on the output. If this indicator is omitted, the following error message is printed:

SYSTEM OF UNITS NOT SPECIFIED. IUNIT NOT ENTERED OR ZERO.

This message merely informs the user of this omission, execution of the problem is not terminated.

b.  $K_{11}$  and  $K_{12}$  cannot be zero simultaneously. Similarly,  $K_{21}$  and  $K_{22}$  cannot be zero simultaneously. These situations lead to an undefined boundary. The error message below results from this case.

**BOTH INDICATORS AT ONE BOUNDARY ARE ZERO**

c.  $K_{12}$  cannot be zero. This is a somewhat artificial restriction imposed by the formulation of the problem. In a physical sense it prevents the possibility of the unsolvable Neuman problem. If  $K_{12}$  is zero the following error message is printed.

**FORMULATION DOES NOT PERMIT  $K_{12}$  TO BE ZERO.**

d. The number of integration intervals must be even. This restriction arises from the computer formulation of Simpson's rule. If an uneven number is entered, the following error message results:

**NUMBER OF INTEGRATION INTERVALS IS NOT EVEN**

e. The computer program generates an error message if the time increment or the length increment is zero or negative. This message reads:

**TIME OR LENGTH INCREMENT IS ZERO OR NEGATIVE**

f. The initial time for each program is zero.

g. The program uses even increments of time and length. The maximum number of length increments is one hundred.

**E. OUTPUT**

The output generated by STASH consists of two segments: the input data display and temperature profiles which are always generated; and the intermediate print which is controlled by the first card in the data deck. After reading the data, STASH prints it out along with suitable titles and headings as shown in Figure 5. If the eigenvalue solution is requested a table of the eigenvalues, and iterations, is printed as shown in Figure 6. Intermediate print options giving the values of the series and the unsteady state produce output as shown in Figure 7 for each station along the slab at each time step. Figure 7 also shows the form of the temperature profiles as generated at each time step.

CASE 4 INSULATED BARRIERY

PHYSICAL CONSTANTS TO DEFINE THE PROBLEM

SYSTEM OF UNITS

LENGTH INCH	0.000000E+00	TEMPERATURE FAHRENHEIT	0.000000E+00	WEIGHT POUND	0.000000E+00	FINAL TIME	0.000000E+00
LENGTH INCH	0.000000E+00	TEMPERATURE FAHRENHEIT	0.000000E+00	WEIGHT POUND	0.000000E+00	FINAL TIME	0.000000E+00
TEMPERATURE FAHRENHEIT	0.000000E+00	WEIGHT POUND	0.000000E+00	LENGTH INCREMENT	0.000000E+00	TEMPERATURE FAHRENHEIT	0.000000E+00
LENGTH INCH	0.000000E+00	TEMPERATURE FAHRENHEIT	0.000000E+00	WEIGHT POUND	0.000000E+00	FINAL TIME	0.000000E+00

BOUNDARY CONDITION INDICATORS FROM THE DIFFERENTIAL EQUATION

K22

K21

K12

K11

0.000000E+01

0.000000E+01

0.000000E+01

MULTIPLYING FACTORS FOR BOUNDARY AND INITIAL CONDITION FUNCTIONS

0.000000E+01

0.000000E+01

0.000000E+01

CALCULATION PARAMETERS

0.000000E+01

0.000000E+01

0.000000E+01

EIGENVALUE SOLUTION PARAMETERS

0.000000E+01

0.000000E+01

0.000000E+01

0.000000E+01

0.000000E+01

0.000000E+01

ALPHA

0.000000E+01

DEFK

0.000000E+01

Figure 8. Sample Output (Case 4) Showing Display of Input

SOLUTION FOR EIGENVALUES

ROOT NO	Z
1	0.15707962E 01
2	9.47123838E 01
3	0.78539814E 01
4	0.10995574E 02
5	0.14137166E 02
6	0.17278759E 02
7	0.20420352E 02
8	0.23561944E 02
9	0.26703537E 02
10	0.29845120E 02

Figure 5. Sample Output (Case 4) Showing Eigenvalue Solution

```

1 0.8000000E 03
2 0.09999999E 02
3 0.09999999E 02
4 0.09999999E 02
5 0.09999999E 02
6 0.09999999E 02
7 0.09999999E 02
8 0.09999999E 02
9 0.09999999E 02
10 0.09999999E 02

SERIES PORTION OF SOLUTION
X= 0.09999999E 02

TERM          SUMMATION
-0.11827815E 03
0.1302856E-03
-0.8489587E-15
0.51741985E-31
0.
-0.
0.
-0.
0.
-0.

UNSTEADY STATE PORTION OF SOLUTION
X
0.09999999E 02
TEMPERATURE DISTRIBUTION ALONG THE ROD AT 1.000 INTERVALS
0.09999999E 04 0.96299432E 03 0.92689987E 03 0.89260542E 03 0.86095545E 03
0.93272925E 03 0.90062185E 03 0.86922683E 03 0.83902174E 03 0.81035632E 03
0.76344399E 03
    
```

Figure 7. Sample Output (Case 4) Showing Intermediate Print

SECTION V  
CONCLUSIONS

Several classes of problems were run to check out the program. The results were compared with a finite-difference heat transfer program (LTA) which was developed by Lockheed Aircraft Corporation. These results were examined for accuracy and speed of convergence.

The intermediate print feature of the program was used to determine the convergence. Examination showed that convergence was quite rapid, usually less than ten terms, for constant boundary conditions, away from time zero. More terms were needed in the vicinity of zero time to produce convergence. For time-varying boundary conditions, the series does not converge very quickly. However, a study of the solution convergence showed that a twenty term series using one hundred integration steps obtained results within one percent of the LTA solution for times exceeding one hundred seconds. At smaller times a fifty term series with one hundred integration steps was required.

Appendix III contains the results of five check problems compared with the results from the LTA finite difference program.

No comparison is made at zero time since the program obtains these values from the initial conditions rather than from a series calculation. The curves are plotted from data generated by the program. Case 1 is the sample problem detailed in Section IV C. All other cases used the same physical parameters.

AFEDL-TR-66-109

APPENDIX I  
COMPUTER PROGRAM SOURCE LISTING

```

@@@JOB STASH      MAP                                STASH001
$IBFYC MAIN      F94/2,XR7                          STASH002
C                                                        STASH003
C      A GENERAL SOLUTION TO THE ONE-DIMENSIONAL HEAT TRANSFER PROBLEM STASH004
C      WITH TIME-DEPENDENT BOUNDARY CONDITIONS AND ARBITRARY INITIAL STASH005
C      CONDITION                                          STASH006
C                                                        STASH007
C      VERSION 2
C      VERSION 2 CALCULATES ZERO TIME USING BOUNDARY AND INITIAL CONDITIONS STASH008
C      VERSION 2 INCORPORATES A MULTIPLIER ON THE INITIAL CONDITION FUNCTION STASH009
C      AND BOUNDARY CONDITION FUNCTIONS TO PERMIT THE USE OF NORMALIZED STASH010
C      FUNCTIONS                                          STASH011
C                                                        STASH012
C      EXTERNAL YFUNC,XFUNC                            STASH013
C      DIMENSION TEMP(100),TITLE(13),EIGEN(100)        STASH014
C      DIMENSION JPRINT(3)                             STASH015
C      DIMENSION NTAB(5)                               STASH016
C      REAL K11BN,K11BN2                               STASH017
C      REAL K11K21,K12K22                              STASH018
C      REAL LHT,L,K,LAMBDA,NUMXSS,NUMSS,KFPHI,KFPHI0,KFPHI1,K11,K12 STASH019
C      I,K21,K22,N,KTERM1,KTERM2                      STASH020
C      COMMON T,X,LAMBDA,KTERM1,KTERM2,ALPHA,BETAN,EXPAN,CBNX,SBMX,DELTA STASH021
C      TX,DELTA,T,K11,K12,K21,K22,FX,NTAB            STASH022
C      COMMON/ROCTS/NTERMS,L,ITERMX,K11K21,K12K22,LIMIT STASH023
C      COMMON/PRINT/JPRINT                            STASH024
C                                                        STASH025
C      FORMAT STATEMENTS                               STASH026
C                                                        STASH027
C      1  FORMAT(12,13A6)                              STASH028
C      2  FORMAT(7E10.0)                                STASH029
C      3  FORMAT(4E10.0)                                STASH030
C      4  FORMAT(3E10.0)                                STASH031
C      5  FORMAT(3I5,5I1)                               STASH032
C      6  FORMAT(E10.0,15)                              STASH033
C      13  FORMAT(1H1,29X,13A6)                         STASH034
C      20  FORMAT(1H0,8X,6HLENGTH,12X,7HTHERMAL,11X,7HDENSITY,10X,8HSPECIFIC, STASH035
C      111X,6HLENGTH,13X,4HTIME,14X,5HFINAL/24X,12HCONDUCTIVITY,28X,4HHEAT STASH036
C      2,11X,9HINCREMENT,9X,9HINCREMENT,12X,4HTIME) STASH037
C      22  FORMAT(1H0,3X,E15.8,3X,E15.0,4X,E15.8,2X,E15.8,3(3X,E15.8)) STASH038
C      30  FORMAT(1HA,35X,60HBOUNDARY CONDITION INDICATORS FROM THE DIFFEREN STASH039
C      TIAL EQUATION//36X,3HK11,16X,3HK12,16X,3HK21,16X,3HK22) STASH040
C      31  FORMAT(1HA,55X,19HMULTIPLYING FACTORS/6+X,3HFOR/45X,40HBOUNDARY AN STASH041
C      IS INITIAL CONDITION FUNCTIONS//30X,4HF(0),30X,4HF(L),30X,4HF(X)//2 STASH042
C      24X,2(E15.8,19X),E15.8) STASH043
C      33  FORMAT(1H0,29X,4(E15.8,4X)) STASH044
C      66  FORMAT(1HA,51X,30HEIGENVALUE SOLUTION PARAMETERS//42X,8HACCURACY,35 STASH045
C      *0X,9HNUMBER OF//44X,5HLIMIT,31X,10HITERATIONS//39X,E15.8,26X,15) STASH046
C      120  FORMAT(28X,4HINCH,14X,4HSLUG,14X,3HSEC,16X,5HPOUND,13X,10HFAHRENHE STASH047
C      117) STASH048
C      130  FORMAT(28X,4HINCH,14X,4HSLUG,14X,3HMIN,16X,5HPOUND,13X,10HFAHRENHE STASH049
C      117) STASH050
C      140  FORMAT(28X,4HINCH,14X,4HSLUG,15X,2HHR,16X,5HPOUND,13X,10HFAHRENHE STASH051
C      117) STASH052
C      150  FORMAT(28X,4HF00T,14X,4HSLUG,14X,3HSEC,16X,5HPOUND,13X,10HFAHRENHE STASH053
C      117) STASH054
C      160  FORMAT(28X,4HF00T,14X,4HSLUG,14X,3HMIN,16X,5HPOUND,13X,10HFAHRENHE STASH055
C      117) STASH056
C      170  FORMAT(28X,4HF00T,14X,4HSLUG,15X,2HHR,16X,5HPOUND,13X,10HFAHRENHE STASH057
C      117) STASH058
C      180  FORMAT(28X,4HINCH,14X,5HPOUND,13X,3HSEC,16X,5HPOUND,13X,10HFAHRENHE STASH059
C      1E117) STASH060
C      190  FORMAT(28X,4HINCH,14X,5HPOUND,13X,3HMIN,16X,5HPOUND,13X,10HFAHRENHE STASH061
C      1E117) STASH062

```

```

303  FORMAT(1HA,54X,22MCALCULATION PARAMETERS//26X,15HNUMBER OF TERMS,1STASH063
15X,19HNUMBER OF INTERVALS,13X,19HNUMBER OF INTERVALS/25X,16HIN THESTASH064
2  SUMMATION,14X,21HFOR THE X INTEGRATION,11X,21HFOR THE Y INTEGRATIONSTASH065
3CN//30X,15,28X,15,26X,15) STASH066
333  FORMAT(1HA,63X,5HALPHA) STASH067
1002 FORMAT(26X,5E15.8) STASH068
1003 FORMAT(1X,E15.8) STASH069
1100 FORMAT(28X,4HINCH,14X,5HPOUND,14X,2HR,16X,5HPOUND,13X,10HFAHRENHSTASH070
1IT) STASH071
1110 FORMAT(28X,4HFCOT,14X,5HPOUND,13X,3HSEC,16X,5HPOUND,13X,10HFAHRENHSTASH072
1EIT) STASH073
1120 FORMAT(28X,4HFCOT,14X,5HPOUND,13X,3HMIN,16X,5HPOUND,13X,10HFAHRENHSTASH074
1EIT) STASH075
1130 FORMAT(28X,4HFCOT,14X,5HPOUND,14X,2HR,16X,5HPOUND,13X,10HFAHRENHSTASH076
1IT) STASH077
1140 FORMAT(1HA,45X,40HPHYSICAL CONSTANTS TO DEFINE THE PROBLEM//59X,15STASH078
1HSYSTEM OF UNITS//27X,6HLENGTH,13X,4HMASS,14X,4HTIME,14X,6HWEIGHT,STASH079
213X,11HTEMPERATURE) STASH080
2002 FORMAT(7X,4HTIME,22X,42HTEMPERATURE DISTRIBUTION ALONG THE ROD AT STASH081
1 ,F3.3,10H INTERVALS) STASH082
3003 FORMAT(1HC) STASH083
3333 FORMAT(1HO,58X,E15.8) STASH084
4004 FORMAT(1HA,63X,4HCEYK) STASH085
4444 FORMAT(1HO,58X,E15.8) STASH086
5000 FORMAT(5I1) STASH087
6100 FORMAT(1H1,25X,2HT=,E15.8,20X,2HX=,E15.8//45X,26HSERIES PORTION OFSTASH088
* SOLUTION//14X,1HN,16X,4HTER=,19X,9HSUMMATION//) STASH089
6110 FORMAT(10X,15,10X,E15.8,10X,E15.8) STASH090
6200 FORMAT(1HO,4CX,34HUNSTEADY STATE PORTION OF SOLUTION//35X,1HX,25X,STASH091
*4HTEMP//) STASH092
6210 FORMAT(28X,F15.8,20X,E15.8) STASH093
1ERROR=0 STASH094
C STASH095
C INTERMEDIATE PRINT OPTIONS STASH096
C STASH097
C READ(5,5000) JPRINT STASH098
C STASH099
C JPRINT=1,PRINT INTERMEDIATE CALCULATIONS. JPRINT=0,DO NOT PRINT. STASH100
C JPRINT(1)-SERIES PORTION OF THE SOLUTION TERM BY TERM STASH101
C JPRINT(2)-UNSTEADY STATE PORTION OF THE SOLUTION STASH102
C JPRINT(3)-SOLUTION FOR THE EIGENVALUES STASH103
C STASH104
C READ (5,1)IUNIT,(TITLE(I),I=1,13) STASH105
C READ(5,2)L,K,RHO,CP,DELTA X,DELTA T,TIMEF STASH106
C READ(5,3)K11,K12,K21,K22 STASH107
C READ(5,4)FO,FL,FY STASH108
C READ(5,5) NTERMS,NSTEPX,NSTEPT,NTAB STASH109
C READ(5,6) LIMIT,ITERMX STASH110
C STASH111
C STASH112
C PRINT INPUT DATA STASH113
C STASH114
C TITLE STASH115
C STASH116
C WRITE (6,21)(TITLE(I),I=1,13) STASH117
C STASH118
C SYSTEM OF UNITS STASH119
C STASH120
C WRITE(6,1140) STASH121
C IF(IUNIT.EQ.0) GO TO 5500 STASH122
C GO TO (102,103,104,105,106,107,108,109,110,111,112,113),IUNIT STASH123
102  WRITE(6,120) STASH124

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103	GO TO 9999 WRITE(6,130) GO TO 9999	STASH125 STASH126
104	WRITE(6,140) GO TO 9999	STASH127 STASH128
105	WRITE(6,150) GO TO 9999	STASH129 STASH130
106	WRITE(6,160) GO TO 9999	STASH131 STASH132
107	WRITE(6,170) GO TO 9999	STASH133 STASH134
108	WRITE(6,180) GO TO 9999	STASH135 STASH136
109	WRITE(6,190) GO TO 9999	STASH137 STASH138
110	WRITE(6,1100) GO TO 9999	STASH139 STASH140
111	WRITE(6,1110) GO TO 9999	STASH141 STASH142
112	WRITE(6,1120) GO TO 9999	STASH143 STASH144
113	WRITE(6,1130) GO TO 9999	STASH145 STASH146
5500	WRITE(6,5550)	STASH147 STASH148
C		STASH149
C	PHYSICAL CONSTANTS	STASH150
C		STASH151
9999	WRITE(6,20) WRITE(6,22) L,K,RHG,CP,DELTA X,DELTA T,TIME F	STASH152 STASH153
C		STASH154
C	BOUNDARY CONDITIONS	STASH155
C		STASH156
	WRITE(6,30) WRITE(6,33) K11,K12,K21,K22	STASH157 STASH158
C		STASH159
C	MULTIPLYING FACTORS	STASH160
C		STASH161
	WRITE(6,51) FO,FL,FX	STASH162
C		STASH163
C	CALCULATION PARAMETERS	STASH164
C		STASH165
	WRITE(6,303) INTERMS,NSTEPX,NSTEPT	STASH166 STASH167
C		STASH168
C	EIGENVALUE SOLUTION PARAMETERS	STASH169
C		STASH170
	WRITE(6,56) LIMIT,IYERMX	STASH171
C		STASH172
C	TEST FOR TABULAR DATA	STASH173
C		STASH174
	DO 50 I=1,5 IF (INTAB(I).NE.0) CALL YASIN(I) CONTINUE	STASH175 STASH176 STASH177
50		STASH178
C		STASH179
C	IF TABLES ARE USED, THEY ARE ASSIGNED AS FOLLOWS	STASH180
C		STASH181
C	NO. 1 FUNCTION PHIC(T)	STASH182
C	NO. 2 FUNCTION PHILE(T)	STASH183
C	NO. 3 FUNCTION PHIPRO(LAMBDA)	STASH184
C	NO. 4 FUNCTION PHIPRL(LAMBDA)	STASH185
C	NO. 5 FUNCTION FOPX(X)	STASH186

C		STASH187
C	ERROR CHECKS ON INPUT DATA	STASH188
C		STASH189
C		STASH190
C	NUMBER OF INTEGRATION STEPS MUST BE EVEN OR ZERO.	STASH191
C	IF ZERO THE PROGRAM SETS THE INTEGRAL EQUAL TO ZERO.	STASH192
C		STASH193
	IF(NSTEPX.EQ.0) GO TO 248	STASH194
	IF(MOD(NSTEPX,2).EQ.0) GO TO 248	STASH195
	WRITE (6,5553)	STASH196
	IERROR=IERROR+1	STASH197
248	IF(NSTEPT.EQ.0) GO TO 249	STASH198
	IF(MOD(NSTEPT,2).EQ.0) GO TO 249	STASH199
	WRITE(6,5553)	STASH200
	IERROR=IERROR+1	STASH201
249	IF((DELTA X.GT.0.)	STASH202
	* .AND.	STASH203
	* (DELTA T.GT.0.))	STASH204
	* GO TO 250	STASH205
	WRITE(6,5551)	STASH206
	IERROR=IERROR+1	STASH207
250	IF(TIMEF.GT.0.) GO TO 251	STASH208
	WRITE(6,5552)	STASH209
	IERROR=IERROR+1	STASH210
C		STASH211
C	K12 CANNOT BE ZERO DUE TO A RESTRICTION IN THE FORMULATION.	STASH212
C		STASH213
251	IF (K12.NE.0.) GO TO 252	STASH214
	WRITE(6,5555)	STASH215
	IERROR=IERROR+1	STASH216
C		STASH217
C	CHECK FOR UNDEFINED BOUNDARY CONDITIONS.	STASH218
C		STASH219
252	IF(((K11.NE.0.).OR.(K12.NE.0.))	STASH220
	* .AND.	STASH221
	* ((K21.NE.0.).OR.(K22.NE.0.)))	STASH222
	* GO TO 253	STASH223
	WRITE(6,44)	STASH224
	IERROR=IERROR+1	STASH225
C		STASH226
253	IF(IERROR.GT.0) STOP	STASH227
C		STASH228
	WRITE(6,333)	STASH229
	PI=3.1415926	STASH230
	ALPHA=K/(RHO*CP)	STASH231
	WRITE(6,3333) ALPHA	STASH232
	DETK=K11*K22-K12*K21	STASH233
	WRITE(6,4004)	STASH234
	WRITE(6,4444) DETK	STASH235
C		STASH236
C	DETERMINE CONSTANTS FOR USE IN DO LOOPS	STASH237
C		STASH238
	CON01=K12*K22*L-DETK	STASH239
	CON01=K11*K12*L	STASH240
	CON02=K11**2	STASH241
	CON03=(K12*L)**2	STASH242
	CON04=FL	STASH243
	CON05=K11*K21	STASH244
	CON06=(K12*K22*(L**2))	STASH245
	CON07=DETK*L	STASH246
	CON08=FO	STASH247
	CON09=K12*FL	STASH248

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CON10=K22*F0
CON11=F0/K12
CON12=K12*DENOM
CON088=K12**2
K11K21=K11*K21
K12K22=K12*K22
C
C DETERMINE EIGENVALUES FOR SERIES SOLUTION
C
IF((K11K21.EQ.0.).AND.(K12K22.EQ.0.))GO TO 400
IF(DELTA.TEQ.300,100
100 CALL SOLVE1(DETK,EIGEN,NTERMS)
GO TO 900
200 CALL SOLVE2(DETK,EIGEN,NTERMS)
GO TO 900
300 CALL SOLVE3(DETK,EIGEN,NTERMS)
GO TO 900
400 CALL SOLVE4(DETK,EIGEN,NTERMS)
C
C SET UP INDICES FOR DO LOOPS
C
900 NTEMP=(TIHFF/DELTA)+1.5
NTEMPX=(L/DELTA)+1.5
WRITE(6,3003)
T=-DELTA
DO 199 N7=1,NTEMP
T=T+DELTA
X=-DELTA
DO 999 N8=1,NTEMPX
IF(T.EQ.0.) GO TO 299
X=X+DELTA
SERIES=0.
IF(JPRINT(1).NE.0) WRITE(6,6100) T,X
C
C SET UP LOOP TO GENERATE SERIES SUMMATION FOR TRANSIENT SOLUTION
C
CO999I=1,NTERMS
ZN=EIGEN(I)
9 BETAN=ZN/L
ZN2=ZN**2
ZOENOM=ZN2*DENOM
SBNX=SIN(BETAN*X)
CBNX=COS(BETAN*X)
SZN=SIN(ZN)
CZN=COS(ZN)
K11B2=K11*BETAN
K11B2=K11B2**2
ZN2SZN=ZN2*SZN
EXPMUL=EXP(-(ALPHA*(BETAN)**2)*T)
SUHCON=BETAN*(K12*SBNX-K11B2*CBNX)/(ZN*(K11B2+CON088)+(K11B2-
1CON088)*SZN+CZN-2.*K11B2*K12*(SZN**2))
KTERM1=((CON01*ZN2SZN-CON02*ZN2SZN+CON03*(ZN*(CZN-SZN)))/ZOENOM)*
1CON04
KTERM2=((CON05*ZN2SZN+CON06*(SZN-ZN)+CON07*ZN*(1.-CZN))/ZOENOM)*
1CON08
KFPHI1=KTERM1*PHI(0.)
KFPHI0=KTERM2*PHI(0.)
KFPHI=EXPMUL*(KFPHI0+KFPHI1)
IF(NSTEPT.EQ.0) GOTO 399
TIHINT=FIAT(0.,T,NSTEPT,TFUNC)
GO TO 599
399 TIHINT=0.
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	DATA PI/3.1415926/	STASH373
	SLOPE =DETK/(K12K22*L)	STASH374
	IF(JPRINT(3).NE.0) WRITE(6,6300)	STASH375
	CO999 I=1, NTERMS	STASH376
	NN=I	STASH377
	IF(K11K21.EQ.0.) GO TO 801	STASH378
	GO TO 799	STASH379
801	IF(ABS(SLOPE).LT.1.0) GO TO 800	STASH380
799	Z0=(2.*NN-1.)*(PI/2.)	STASH381
	GO TO 850	STASH382
800	Z0=(2.*NN+1.)*(PI/2.)	STASH383
850	BOUND=0.0	STASH384
	CO 99 I=1, ITERMX	STASH385
	U=DETK*L*Z0/(K11K21*Z0**2+K12K22*L**2)	STASH386
	IF(ABS(SLOPE).LT.1.0) GO TO 860	STASH387
	Z1=(NN-1.)*PI+ATAN(U)	STASH388
	GO TO 870	STASH389
860	Z1=NN*PI+ATAN(U)	STASH390
870	IF(ABS(Z1-Z0).LT.LIMIT) GO TO 9	STASH391
	IF(BOUND.EQ.(Z1-Z0)) GO TO 90	STASH392
	BOUND=Z1-Z0	STASH393
	Z0=Z1	STASH394
	IF(JPRINT(3).NE.0) WRITE(6,6310) I,J,U,Z1	STASH395
99	CONTINUE	STASH396
	WRITE(6,11) I, ITERMX	STASH397
	STOP	STASH398
9	EIGEN(I)=Z1	STASH399
	GO TO 999	STASH400
90	EIGEN(I)=(Z1+Z0)/2.0	STASH401
999	CONTINUE	STASH402
	RETURN	STASH403
C		STASH404
C	ERRCR MESSAGES	STASH405
C		STASH406
11	FORMAT(10X,12HROOT NUMBER ,J1,23HDO NOT CONVERGE IN 100 ITERATIONS)	STASH407
	END	STASH408
66		STASH409
618FTC	SOLV2 #94/2,XR7	STASH410
	SUBROUTINE SOLVE2(DETK,E/2,NTERMS)	STASH411
C		STASH412
C	SOLVES TAN(Z)=-D*L*Z/(K11*Z**2+K22*K12*L**2)	STASH413
C		STASH414
		STASH415
	DIMENSION EIGEN(NTERMS)	STASH416
	DIMENSION JPRINT(3)	STASH417
	DIMENSION NYAB(5)	STASH418
	REAL K11K21,K12K22,L,K11,K12,NN	STASH419
	REAL LIMIT,L,K,LAMBDA,ITERMS,NUMS1,KFPH1,KFPH10,KFPH1L,K11,K12	STASH420
	I,K21,K22,N,KTERMI,KTERK2	STASH421
	COMMON Y,X,LAMBDA,KTERK2,KFPH1,ALPHA,BSTAN,EXOMUL,CORR,SNMX,DELTA	STASH422
	IX,DELTAT,K11,K12,K21,K22,FE,FIAB	STASH423
	COMMON/ROOTS/NTERMS,L,I,ITERMX,K11K21,K12K22,LIMIT	STASH424
	COMMON/PRINT/JPRINT	STASH425
6300	FORMAT(10X,12HROOT NUMBER ,J1,23HDO NOT CONVERGE IN 100 ITERATIONS)	STASH426
6310	FORMAT(28X,13,23HDO NOT CONVERGE IN 100 ITERATIONS)	STASH427
	DATA PI/3.1415926/	STASH428
	IF(JPRINT(3).NE.0) WRITE(6,6300)	STASH429
	CO999 I=1, NTERMS	STASH430
	NN=I	STASH431
	Z0=(NN+1.)*PI	STASH432
850	BOUND=0.0	STASH433
		STASH434

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DO 99 J=1,ITERMX
U=DETK*L*Z0/(K11K21*Z0**2+K12K22*L**2)
Z1=(NN*PI)+ATAN(U)
IF(ABS(Z1-Z0).LT.LIMIT) GO TO 9
IF(BOUND.EQ.(Z1-Z0)) GO TO 90
BOUND=Z1-Z0
Z0=Z1
IF(JPRINT(3).NE.0) WRITE(6,6310) I,J,U,Z1
99 CONTINUE
WRITE(6,11) I,ITERMX
STOP
9 EIGEN(I)=Z1
GO TO 999
90 EIGEN(I)=(Z1+Z0)/2.0
999 CONTINUE
RETURN
C
C ERROR MESSAGES
C
11 FORMAT(10X,12HROOT NUMBER ,I3,22HDID NOT CONVERGE AFTER,I5,11H ITERATIONS)
END
$*
$IBFTC SOLV3 P94/2,XR7
SUBROUTINE SOLVE3(DETK,EIGEN,NTERMS)
C
C SOLVES TAN(Z)=0.0
C
DIMENSION EIGEN(NTERMS)
DIMENSION JPRINT(3)
DIMENSION NTAB(5)
REAL K11K21,K12K22,L,LIMIT,NN
REAL LIMIT,L,K,LAMBDA,NUMXSS,NUMSS,KFPHI,KFPHIO,KFPHIL,K11,K12
I,K2C,K22,h,KTERM1,KTERM2
COMMON T,X,LAMBDA,KTERM1,KTERM2,ALPHA,BETAN,EXPUL,CBNX,SENX,DELTA
IX,DELTAT,K11,K12,K21,K22,FX,NTAB
COMMON/ROOTS/NTERMS,L,ITERMX,K11K21,K12K22,LIMIT
COMMON/PRINT/JPRINT
6300 FORMAT(1H1,46X,24HSOLUTION FOR EIGENVALUES//26X,7HROOT NO,49X,1HZ)
6320 FORMAT(28X,I3,44X,E15.8)
DATA FT/3,1415926/
IF(JPRINT(3).NE.0) WRITE(6,6300)
DO 999 I=1,NTERMS
NN=I
Z1=NN*PI
EIGEN(I)=Z1
IF(JPRINT(3).NE.0) WRITE(6,6320) I,Z1
999 CONTINUE
RETURN
$*
$IBFTC SOLV4 P94/2,XR7
SUBROUTINE SOLVE4(DETK,EIGEN,NTERMS)
C
C SOLVES TAN(Z)= INFINITY
C
DIMENSION EIGEN(NTERMS)
DIMENSION NTAB(5)
DIMENSION JPRINT(3)
REAL K11K21,K12K22,L,LIMIT,NN
REAL LIMIT,L,K,LAMBDA,NUMXSS,NUMSS,KFPHI,KFPHIO,KFPHIL,K11,K12
I,K21,K22,N,KTERM1,KTERM2

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COMMON T,X,LAMBDA,KTERM1,KTERM2,ALPHA,BETAN,EXPUL,CBNX,SBNX,DELTA STASH497
IX,DELTAT,K11,K12,K21,K22,FX,NTAB STASH498
COMMON/ROOTS/NTERMS,L,IYERMX,K11K21,K12K22,LIMIT STASH499
COMMON/PRINT/JPRINT STASH500
0300 FORMAT(1H1,46X,24F,SOLUTION FOR EIGENVALUES//26X,7HROOT NO,49X,1H2) STASH501
6320 FORMAT(28X,13,44X,E15.8) STASH502
DATA PI/3.1415926/ STASH503
IF(JPRINT(3).NE.0) WRITE(6,6300) STASH504
DO 999 I=1,NTERMS STASH505
  NN=I STASH506
  ZI=((2.*NN-1.)*PI)/2.0 STASH507
  EIGEN(I)=ZI STASH508
  IF(JPRINT(3).NE.0) WRITE(6,6320)I,ZI STASH509
999 CONTINUE STASH510
  RETURN STASH511
  END STASH512
$S
$IBPTC SIMPS  P94/2,XR7 STASH513
  REAL FUNCTION FINT(A,B,NN,F) STASH514
  C SIMPSON METHOD STASH516
  C A=LOWER BOUND STASH517
  C B=UPPER BOUND STASH518
  C NN=NUMBER OF INTERVALS, MUST BE EVEN STASH519
  C F=FUNCTION TO BE INTEGRATED, FUNCTION NAME MUST BE DECLARED STASH520
  C EXTERNAL STASH521
  C STASH522
  REAL LIMIT,L,K,LAMBDA,NUMXSS,NUMSS,XFPHI,KFPHIO,KFPHIL,K11,K12
  I,K21,K22,N,KTERM1,KTERM2 STASH524
  COMMON T,X,LAMBDA,KTERM1,KTERM2,ALPHA,BETAN,EXPUL,CBNX,SBNX,DELTA STASH525
  IX,DELTAT,K11,K12,K21,K22,FX,NTAB STASH526
  FN=NN STASH527
  H=(B-A)/FN STASH528
  SUMA=0.0 STASH529
  SUMB=0.0 STASH530
  F=FN-1 STASH531
  COIOJ=1,H,2 STASH532
  FJ=F
  XX=FJ*H STASH533
10 SUMA=SUMA+F(XX) STASH534
  F=FN-2 STASH535
  CO2OKK=2,H,2 STASH536
  FK=FK
  XX=FK*H STASH537
  SUMB=SUMB+F(XX) STASH538
20 CONTINUE STASH539
  FINT=(H/3.)*((F(A)+F(B)+4.*SUMA+2.*SUMB)) STASH540
  RETURN STASH541
  END STASH542
$S
$IBPTC FUNCX  P94/2,XR7 STASH543
  FUNCTION XFUNC(XX) STASH544
  C THIS FUNCTION SETS UP THE INTEGRAND FOR THE / INTEGRAL STASH549
  C STASH550
  C DIMENSION NTAB(5) STASH551
  REAL LIMIT,L,K,LAMBDA,NUMXSS,NUMSS,XFPHI,KFPHIO,KFPHIL,K11,K12 STASH552
  I,K21,K22,N,KTERM1,KTERM2 STASH553
  COMMON T,X,LAMBDA,KTERM1,KTERM2,ALPHA,BETAN,EXPUL,CBNX,SBNX,DELTA STASH554
  IX,DELTAT,K11,K12,K21,K22,FX,NTAB STASH555
  BNXX=BETAN*XX STASH556
  XFUNC=EXPUL*(K12*SIN(BNXX))-K11*BETAN*COS(BNXX)+FX*FOPX(XX) STASH557
  STASH558

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RETURN                                     STASH559
END                                         STASH560
**                                          STASH561
$IBFTC FUNCT #94/2,XRT                     STASH562
FUNCTION TFUNC(LAMBDA)                     STASH563
C                                          STASH564
C THIS FUNCTION SETS UP THE INTEGRAND FOR THE LAMBDA INTEGRAL STASH565
C                                          STASH566
REAL LIMIT,L,K,LAMBDA,NUNXSS,NUNXS,KFPHI,KFPDIO,KFPHIL,KI1,KI2 STASH567
1,K21,K22,N,KYERN1,KYERN2                 STASH568
COMMON T,X,LAMBDA,KYERN1,KYERN2,ALPHA,BETAN,EXPMUL,CONX,SBNX,DELTA STASH569
IX,DELTAI,KI1,KI2,K21,K22,FX,NTAB       STASH570
TERN1=KYERN1*PHIPR1(LAMBDA)             STASH571
TERN2=KYERN2*PHIPR1(LAMBDA)             STASH572
TFUNC=(TERN1+TERN2)*EXP{(ALPHA*(BETAN)**2)*(LAMBDA-T)} STASH573
RETURN                                     STASH574
END                                         STASH575
**                                          STASH576
$IBFTC TABLE #94/2,XRT                     STASH577
SUBROUTINE TABIN(I)                         STASH578
C                                          STASH579
C READS IN TABULAR DATA                   STASH580
C                                          STASH581
1  FORMAT(I5,2F10.0,55H                    STASH582
   =)                                       STASH583
2  FORMAT(1HA,61X,9HTABLE NO.,I2)         STASH584
3  FORMAT(1HD,50X,34INDEPENDENT           DEPENDENT/51X,33H VARI STASH585
   *BLE VARIABLE)                          STASH586
4  FORMAT(48X,E15.8,16X,E15.8)           STASH587
REAL INVAR                                  STASH588
DIMENSION NTAB(5)                           STASH589
DIMENSION NTABLE(5),INDVAR(5,50),DEPVAR(5,50) STASH590
COMMON/PTDATA/ INVAR,DEPVAR              STASH591
READ(5,1) NTABLE(I)                         STASH592
WRITE(6,2) NTABLE(I)                       STASH593
WRITE(6,3)                                  STASH594
DO 150 J=1,50                               STASH595
  READ(5,1)N,INDVAR(I,J),DEPVAR(I,J)       STASH596
  IF(NTABLE(I)*N) 50,100,110              STASH597
  WRITE(6,4) INDVAR(I,J),DEPVAR(I,J)       STASH598
110 CONTINUE                                STASH599
  WRITE(6,5) NTABLE(I)                     STASH600
100 RETURN                                  STASH601
50  WRITE(6,6)                              STASH602
STOP                                         STASH603
C                                          STASH604
C                                          STASH605
C          ERROR MESSAGES                  STASH606
C                                          STASH607
5  FORMAT(1HA,41X,9HTABLE NO.,I2,29H CONTAINS MORE THAN 50 POINTS) STASH608
6  FORMAT(1HA,48X,27ERROR (N TABULAR INPUT DATA) STASH609
   END                                       STASH610
**                                          STASH611
$IBFTC INTERP #94/2,XRT                     STASH612
REAL FUNCTION INTERP(TX,I)                 STASH613
C                                          STASH614
C LINEAR INTERPOLATION FOR TABULAR DATA STASH615
C                                          STASH616
DIMENSION NTAB(5)                           STASH617
DIMENSION INVAR(5,50),DEPVAR(5,50)       STASH618
COMMON/PTDATA/ INVAR,DEPVAR              STASH619
REAL INVAR                                  STASH620
DO 10 J=1,50

```

```

      IF(TX-INDVAR(L,J)) 20,30,10
10  CONTINUE
      WRITE(6,99) I
      CALL EXIT
20  INTERP=DEPVAR(I,J-1)+(DEPVAR(I,J)-DEPVAR(I,J-1))*(TX-INDVAR(I,J-1)
      *)/(INDVAR(L,J)-INDVAR(I,J-1))
      GO TO 100
30  INTERP=DEPVAR(I,J)
100 RETURN
C
C          ERROR MESSAGES
C
99  FORMAT(10X,35HARGUMENT EXCEEDS EXTENT OF TABLE NO.,I2)
      END
$*
$IBFTC PHIO  #94/2,XR7
      FUNCTION PHIO(TT)
C
C  THIS FUNCTION CALCULATES THE INSTANTANEOUS VALUE OF THE
C  TIME-VARYING BOUNDARY CONDITION AT X=0.
C  THE FUNCTION PHIO(T) MAY BE LOADED INTO THE PROGRAM
C  AS AN ANALYTICAL EXPRESSION OR AS POINT DATA IN
C  TABULAR FORM
C
      REAL INTERP
      REAL LIMIT,L,K,LAMBDA,NUMXSS,NUMSS,KFPHI,KFPHIO,KFPHIL,K11,K12
      I,K21,K22,N,KTERM1,KTERM2
      COMMON T,X,LAMBDA,KTERM1,KTERM2,ALPHA,BETAN,EXPMUL,CBNX,SBNX,DELTA
      IX,DELTAT,K11,K12,K21,K22,FX,NTAB
      DIMENSION NTAB(5)
      IF(NTAB(1).NE.0) GO TO 100
C
C  PHIO=ANY FUNCTION OF TIME
C
      PHIO=1.0
      RETURN
100 PHIO=INTERP(TT,1)
      RETURN
      END
$*
$IBFTC PHIL  #94/2,XR7
      FUNCTION PHIL(TT)
C
C  THIS FUNCTION CALCULATES THE INSTANTANEOUS VALUE OF THE
C  TIME-VARYING BOUNDARY CONDITION AT X=L.
C  THE FUNCTION PHIL(T) MAY BE LOADED INTO THE PROGRAM
C  AS AN ANALYTICAL EXPRESSION OR AS POINT DATA IN
C  TABULAR FORM.
C
      REAL INTERP
      REAL LIMIT,L,K,LAMBDA,NUMXSS,NUMSS,KFPHI,KFPHIO,KFPHIL,K11,K12
      I,K21,K22,N,KTERM1,KTERM2
      COMMON T,X,LAMBDA,KTERM1,KTERM2,ALPHA,BETAN,EXPMUL,CBNX,SBNX,DELTA
      IX,DELTAT,K11,K12,K21,K22,FX,NTAB
      DIMENSION NTAB(5)
      IF(NTAB(2).NE.0) GO TO 100
C
C  PHIL=ANY FUNCTION OF
C
      PHIL=1.
      RETURN
100 PHIL=INTERP(TT,2)

```

RETURN	STASH683
END	STASH684
*=	STASH685
#IBFTC DERIVO #94/2,XR7	STASH686
FUNCTIONPHIPRO(LAMBDA)	STASH687
C	STASH688
C THIS FUNCTION CALCULATES THE INSTANTANEOUS VALUE OF THE	STASH689
C DERIVATIVE OF THE TIME-VARYING BOUNDARY CONDITION AT X=0.	STASH690
C THE FUNCTION MAY BE LOADED ANALYTICALLY OR AS POINT	STASH691
C DATA IN TABULAR FORM.	STASH692
C	STASH693
REAL INTERP	STASH694
REAL LIMIT,L,K,LAMBDA,NUMXSS,NUMSS,KFPHI,KFPHIO,KFPHIL,K11,K12	STASH695
I,K21,K22,N,KTERM1,KTERM2	STASH696
COMMON T,X,LAMBDA,KTERM1,KTERM2,ALPHA,BETAN,EXPMUL,CBNX,SBNX,DELTA	STASH697
IX,DELTAT,K11,K12,K21,K22,FX,NTAB	STASH698
DIMENSION NTAB(5)	STASH699
IF(NTAB(3).NE.0) GO TO 100	STASH700
C	STASH701
C PHIPRO=ANY FUNCTION OF TIME	STASH702
C	STASH703
PHIPRO=0.	STASH704
RETURN	STASH705
100 PHIPRO=INTERP(LAMBDA,3)	STASH706
RETURN	STASH707
END	STASH708
*=	STASH709
#IBFTC DERIVL #94/2,XR7	STASH710
FUNCTIONPHIPRL(LAMBDA)	STASH711
C	STASH712
C THIS FUNCTION CALCULATES THE INSTANTANEOUS VALUE OF THE	STASH713
C DERIVATIVE OF THE TIME-VARYING BOUNDARY CONDITIONS AT X=L.	STASH714
C THE FUNCTION MAY BE LOADED ANALYTICALLY OR AS POINT DATA	STASH715
C IN TABULAR FORM	STASH716
C	STASH717
REAL INTERP	STASH718
REAL LIMIT,L,K,LAMBDA,NUMXSS,NUMSS,KFPHI,KFPHIO,KFPHIL,K11,K12	STASH719
I,K21,K22,N,KTERM1,KTERM2	STASH720
COMMON T,X,LAMBDA,KTERM1,KTERM2,ALPHA,BETAN,EXPMUL,CBNX,SBNX,DELTA	STASH721
IX,DELTAT,K11,K12,K21,K22,FX,NTAB	STASH722
DIMENSION NTAB(5)	STASH723
IF(NTAB(4).NE.0) GO TO 100	STASH724
C	STASH725
C PHIPRL=ANY FUNCTION OF TIME	STASH726
C	STASH727
PHIPRL=0.	STASH728
RETURN	STASH729
100 PHIPRL=INTERP(LAMBDA,4)	STASH730
RETURN	STASH731
END	STASH732
*=	STASH733
#IBFTC FX #94/2,XR7	STASH734
FUNCTIONFCFX(L)	STASH735
C	STASH736
C THIS FUNCTION COMPUTES THE INITIAL CONDITIONS OF THE ROD.	STASH737
C THESE INITIAL CONDITIONS MAY BE LOADED INTO THE PROGRAM	STASH738
C ANALYTICALLY OR AS POINT DATA IN TABULAR FORM.	STASH739
C	STASH740
REAL INTERP	STASH741
REAL LIMIT,L,K,LAMBDA,NUMXSS,NUMSS,KFPHI,KFPHIO,KFPHIL,K11,K12	STASH742
I,K21,K22,N,KTERM1,KTERM2	STASH743
COMMON T,X,LAMBDA,KTERM1,KTERM2,ALPHA,BETAN,EXPMUL,CBNX,SBNX,DELTA	STASH744

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```
      XX, DELTAF, N11, K12, K21, K22, FX, NYAB  
      DIMENSION NYAB(5)  
      IF (NYAB(5).NE.0) GO TO 100  
C  
C      FDFX= ANY FUNCTION OF X  
C  
      FDFX=1.  
55  RETURN  
100 FDFX=INTERP(XX,5)  
      RETURN  
      END
```

```
STASH745  
STASH746  
STASH747  
STASH748  
STASH749  
STASH750  
STASH751  
STASH752  
STASH753  
STASH754  
STASH755
```

APPENDIX II  
EIGENVALUE SUBROUTINES

APPENDIX II  
EIGENVALUE SUBROUTINES

The solution of equation 53 depends on values of  $\beta_n$  and which are derived from the positive eigenvalues of Equation 40.

$$\tan z_n = \frac{D L Z_n}{K_{21} K_{11} Z_n^2 + K_{22} K_{12} L^2} \quad (40)$$

Since we are seeking positive values of  $z_n$  the sign of the left-hand side of the equation may be associated with the parameter, D. Thus three formulations are possible corresponding to D being positive, negative or zero. A fourth possibility is that of the denominator going to zero. The last two solutions are trivial. If D is zero we have

$$\tan z_n = 0$$

The solution to this equation is merely

$$z_n = n \pi \quad (54)$$

If the denominator of equation 40 goes to zero we have

$$\tan z_n = \infty$$

The solution to the equation is

$$z_n = \frac{(2n-1)\pi}{2} \quad (55)$$

However, if D has a value other than zero the equations are solved by an iterative process. In these cases the eigenvalue subroutine has been programmed to ignore the root at (0,0) since this produces a trivial solution. The procedure then is outlined below for a positive value of D.

We know that the solution lies between

$$\left[ (n-1)\pi, \frac{(2n-1)\pi}{2} \right], \quad n = 1, 2, 3, \dots$$

For a first approximation to the root,  $z_{n,0}$ , we shall choose

$$z_{n,0} = \frac{(2n-1)\pi}{2} \quad (56)$$

We then write two equations

$$u_{n,m} = \frac{D L Z_{n,m-1}}{K_{21} K_{11} Z_{n,m-1}^2 + K_{22} K_{12} L^2} \quad (57)$$

$$Z_{n,m} = (n-1)\pi + \tan^{-1}(u_{n,m}) \quad (58)$$

Where the subscripts n and m refer to the m<sup>th</sup> iteration toward the n<sup>th</sup> root. The root is then determined to any desired LIMIT of accuracy by writing

$$Z_{n,m} - Z_{n,m-1} < \text{LIMIT} \quad (59)$$

Provision is made in the program to print out the iteration steps should any trouble occur. The basic difference in the solution for a negative value of D arises in the first approximation,  $Z_{n,0}$ . For negative values of D Equation 56 becomes

$$Z_{n,0} = (n + 1) \pi \quad (60)$$

and the solution proceeds as before with Equation 58 becoming

$$Z_{n,m} = n\pi + \tan^{-1}(u_{n,m}) \quad (61)$$

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APPENDIX III

RESULTS OF CHECK PROBLEMS

TABLE II  
COMPARISON OF DATA FOR CASE I

T(0,t)=t; T(L,t)=0; T(x,0)=0							
L	TEMP @	TEMP @ t=50		TEMP @ t=500		TEMP @ t=1000	
	t=0	STASH	LTA	STASH	LTA	STASH	LTA
0.0	0.00	50.00	50.00	500.00	500.00	1000.00	1000.00
0.5	0.00	37.39	37.38	455.95	455.93	930.71	930.69
1.0		27.45	27.46	414.85	414.83	864.38	864.35
1.5		19.79	19.80	376.56	376.53	800.87	800.83
2.0		13.99	14.00	340.92	340.87	740.02	739.97
2.5		9.76	9.70	307.74	307.69	681.66	681.60
3.0		6.58	6.59	276.88	276.83	625.65	625.59
3.5		4.37	4.38	248.18	248.12	571.82	571.76
4.0		2.84	2.85	221.48	221.42	520.03	519.96
4.5		1.80	1.81	196.61	196.56	470.11	470.04
5.0		1.12	1.13	173.43	173.37	421.90	421.84
5.5		0.68	0.68	151.77	151.72	375.26	375.20
6.0		0.40	0.41	131.43	131.43	330.03	329.97
6.5		0.23	0.24	112.44	112.36	286.04	285.99
7.0		0.13	0.13	94.38	94.34	243.15	243.10
7.5		0.07	0.07	77.27	77.24	201.19	201.15
8.0		0.04	0.04	60.91	60.89	160.02	159.98
8.5		0.02	0.02	45.16	45.14	119.47	119.44
9.0		0.01	0.01	29.86	29.84	79.38	79.37
9.5		0.00	0.00	14.85	14.84	39.61	39.60
10.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00

TABLE III

COMPARISON OF DATA FOR CASE 2

T(0,t)=100+t; T(L,t)=10 <sup>2</sup> ; T(x,0)=10 <sup>2</sup>							
L	TEMP @	TEMP @ t=50		TEMP @ t=500		TEMP @ t=1000	
	t=0	STASH	LTA	STASH	LTA	STASH	LTA
0.0	100.00	150.00	150.00	600.00	600.00	1160.00	1100.00
0.5	100.00	137.38	137.38	555.95	555.93	1030.71	1030.69
1.0		127.45	127.46	514.85	514.83	964.38	964.35
1.5		119.79	119.80	476.56	476.53	900.87	900.83
2.0		113.99	114.00	440.92	440.87	840.02	839.97
2.5		109.70	109.70	407.74	407.69	781.66	781.60
3.0		106.58	106.59	376.88	376.83	725.55	725.50
3.5		104.37	104.38	348.18	348.12	671.82	671.76
4.0		102.84	102.85	321.48	321.42	620.03	619.96
4.5		101.80	101.81	296.61	296.56	570.11	570.04
5.0		101.11	101.13	273.43	273.37	521.40	521.34
5.5		100.68	100.68	251.77	251.72	475.76	475.70
6.0		100.40	100.40	231.48	231.43	430.03	429.97
6.5		100.23	100.24	212.40	212.36	386.04	385.99
7.0		100.13	100.13	194.38	194.34	343.15	343.10
7.5		100.07	100.07	177.27	177.24	301.19	301.15
8.0		100.04	100.04	160.91	160.88	260.02	259.98
8.5		100.02	100.02	145.16	145.14	219.47	219.44
9.0		100.01	100.01	129.36	129.34	179.38	179.37
9.5		100.00	100.00	114.85	114.85	139.61	139.60
10.0	100.00	100.00	100.00	100.00	100.00	100.00	100.00

TABLE IV  
COMPARISON OF DATA FOR CASE 3

$T(0,t)=t; T(L,t)=10^2; T(x,0)=\frac{100x}{L}$							
L	TEMP @	TEMP @ t=50		TEMP @ t=500		TEMP @ t=1000	
	t=0	STASH	LTA	STASH	LTA	STASH	LTA
0.0	0.00	50.00	50.00	500.00	500.00	1000.00	1000.00
0.5	5.00	42.38	42.38	460.95	460.93	935.71	935.69
1.0	10.00	37.46	37.46	424.85	424.83	874.38	874.35
1.5	15.00	34.79	34.80	391.56	391.53	815.87	815.83
2.0	20.00	33.99	34.00	360.92	360.87	760.02	759.97
2.5	25.00	34.70	34.70	332.74	332.69	706.66	706.60
3.0	30.00	36.58	36.59	306.88	306.83	655.65	655.59
3.5	35.00	39.37	39.38	283.18	283.16	606.82	606.76
4.0	40.00	42.84	42.85	261.48	261.42	560.03	559.96
4.5	45.00	46.80	46.81	241.61	241.56	515.11	515.04
5.0	50.00	51.11	51.13	223.43	223.37	471.90	471.84
5.5	55.00	55.68	55.68	206.77	206.72	430.26	430.20
6.0	60.00	60.40	60.41	191.48	191.43	390.03	389.97
6.5	65.00	65.23	65.24	177.40	177.36	351.04	350.99
7.0	70.00	70.13	70.13	164.38	164.34	313.15	313.10
7.5	75.00	75.07	75.07	152.27	152.24	276.19	276.15
8.0	80.00	80.04	80.04	140.91	140.89	240.02	239.98
8.5	85.00	85.02	85.02	130.16	130.14	204.47	204.44
9.0	90.00	90.01	90.01	119.86	119.84	169.38	169.37
9.5	95.00	95.00	95.00	109.85	109.84	134.61	134.60
10.0	100.00	100.00	100.00	100.00	100.00	100.00	100.00

COMPARISON OF A... FOR CASE 1

$T(0,t)=t; T(L,t)=100; T(x,0)=\frac{100x}{L}$

L	TEMP @	TEMP @ t=50		TEMP @ t=100		TEMP @ t=100	
	t=0	STASH	LTA	STASH	LTA	STASH	LTA
0.0	0.00	50.00	50.00	500.00	500.00	1000.00	1000.00
0.5	5.00	42.38	42.38	460.95	460.95	935.71	935.99
1.0	10.00	37.46	37.46	424.85	424.83	811.38	811.74
1.5	15.00	34.79	34.80	391.56	391.57	715.37	715.83
2.0	20.00	33.99	34.00	360.92	360.87	660.02	657.97
2.5	25.00	34.70	34.70	332.74	332.69	606.66	606.60
3.0	30.00	36.58	36.59	306.88	306.83	555.65	555.59
3.5	35.00	39.37	39.38	283.18	283.16	506.82	506.76
4.0	40.00	42.84	42.85	261.48	261.42	460.03	459.96
4.5	45.00	46.80	46.81	241.61	241.56	415.11	415.04
5.0	50.00	51.11	51.13	223.43	223.37	371.90	371.84
5.5	55.00	55.68	55.68	206.77	206.72	330.26	330.20
6.0	60.00	60.40	60.41	191.48	191.43	290.03	289.97
6.5	65.00	65.23	65.24	177.40	177.36	251.04	250.99
7.0	70.00	70.12	70.13	164.38	164.34	213.15	213.10
7.5	75.00	75.07	75.07	152.27	152.24	176.19	176.15
8.0	80.00	80.04	80.04	140.91	140.89	140.02	139.98
8.5	85.00	85.02	85.02	130.16	130.14	104.47	104.44
9.0	90.00	90.01	90.01	119.86	119.84	69.38	69.37
9.5	95.00	95.00	95.00	109.85	109.84	34.61	34.60
10.0	100.00	100.00	100.00	100.00	100.00	0.00	0.00

TABLE V

COMPARISON OF DATA FOR CASE 4

T(0,t)=1000; q(L,t)=0; T(x,0)=100							
L	TEMP @	TEMP @ t=300		TEMP @ t=1800		TEMP @ t=3600	
	t=0	STASH	LTA	STASH	LTA	STASH	LTA
0.0	100.00	1000.00	1000.00	1000.00	1000.00	1000.00	1000.00
1.0	100.00	899.95	899.90	994.85	994.40	999.85	999.80
2.0	100.00	802.53	802.50	989.83	989.45	999.71	999.65
3.0	100.00	710.26	709.99	985.06	984.72	999.57	999.53
4.0	100.00	625.48	625.30	980.06	978.98	999.44	999.41
5.0	100.00	550.27	550.05	976.72	976.13	999.33	999.27
6.0	100.00	486.38	486.14	973.37	972.66	999.24	999.19
7.0	100.00	435.25	434.97	970.67	970.04	999.16	999.12
8.0	100.00	397.92	397.52	968.69	968.08	999.10	999.06
9.0	100.00	375.51	375.02	967.49	967.10	999.07	999.01
10.0	100.00	367.70	367.56	967.08	966.99	999.05	998.99

TABLE VI

COMPARISON OF DATA FOR CASE 5

T(0,t)=0; q(L,t) = $\frac{1 \text{ Btu}}{\text{in}^2 \text{ sec}}$ ; T(x,0)=0							
L	TEMP @	TEMP @ t=300		TEMP @ t=1800		TEMP @ t=3600	
	t=0	STASH	LTA	STASH	LTA	STASH	LTA
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.0	0.0	129.76	129.08	416.41	416.34	431.70	431.69
2.0	0.0	266.80	265.45	833.21	833.08	863.41	863.39
3.0	0.0	418.26	416.26	1250.77	1250.58	1295.14	1295.12
4.0	0.0	590.98	588.36	1669.46	1669.22	1726.91	1726.88
5.0	0.0	791.36	788.17	2089.61	2089.32	2158.72	2158.68
6.0	0.0	1025.20	1021.51	2511.51	2511.17	2592.57	2590.54
7.0	0.0	1297.54	1293.43	2935.41	2935.04	3022.49	3022.45
8.0	0.0	1612.46	1608.04	3361.52	3361.12	3454.47	3454.47
9.0	0.0	1973.03	1968.41	3789.99	3789.57	3885.51	3885.47
10.0	0.0	2381.11	2376.43	4220.90	4220.48	4318.69	4318.58

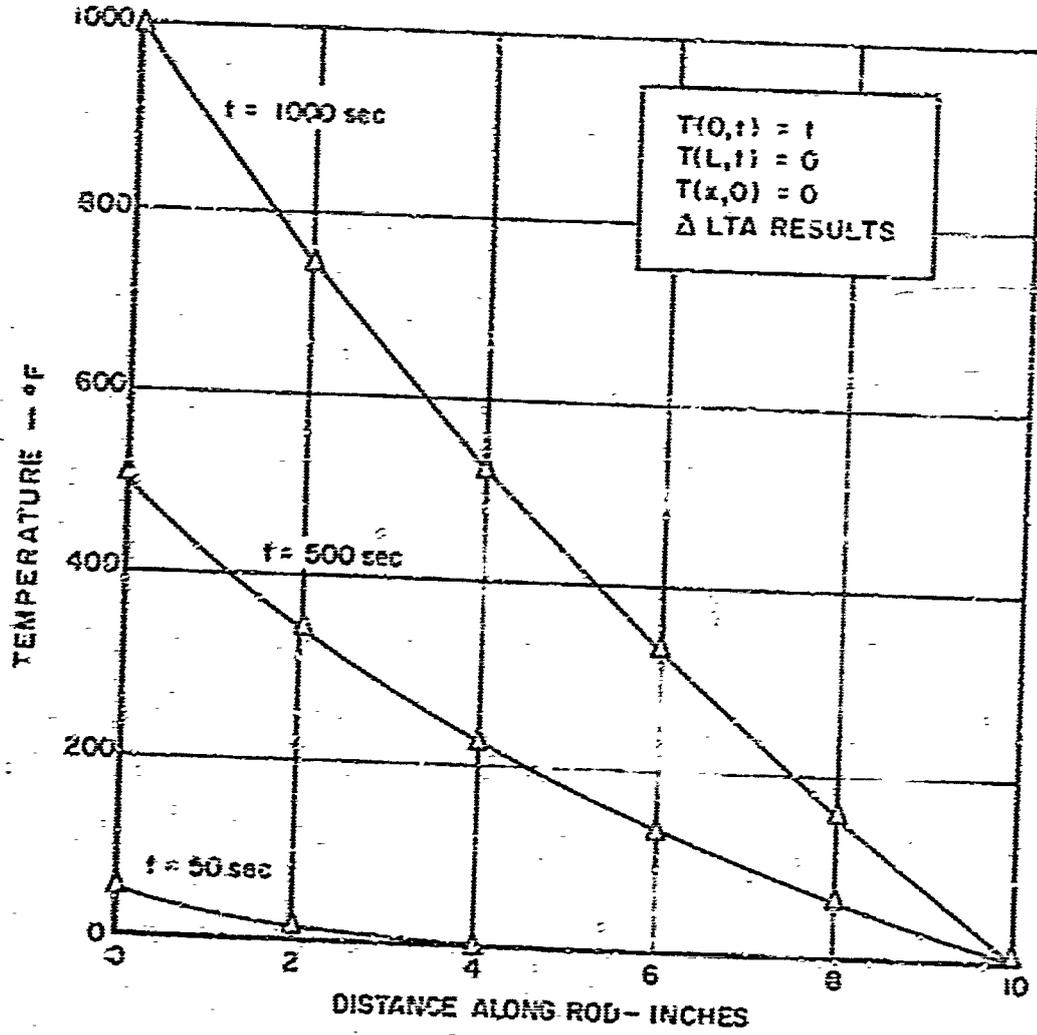


Figure 8. Temperature Profiles (Case 1)

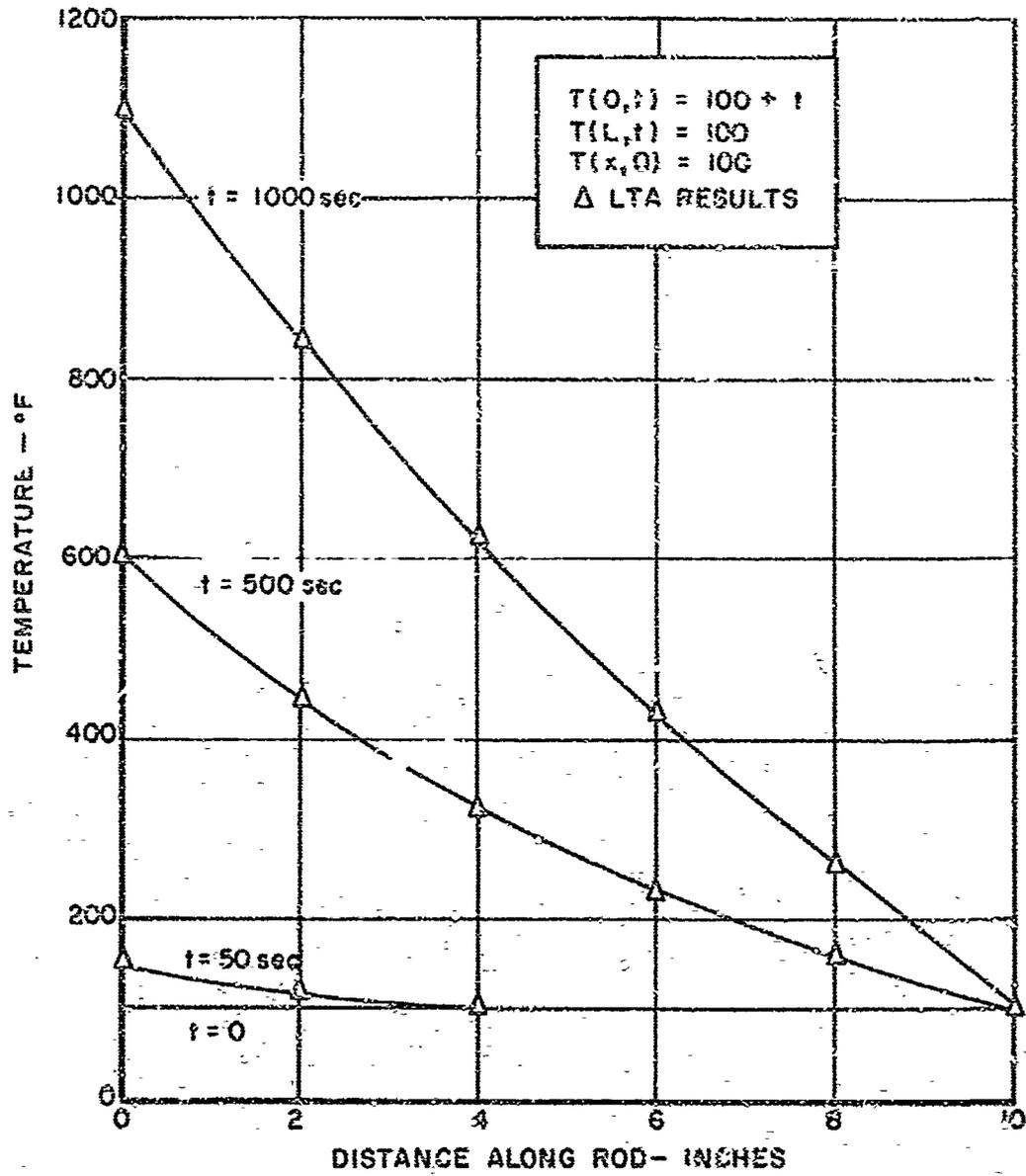


Figure 2. Temperature Profiles (Case 2)

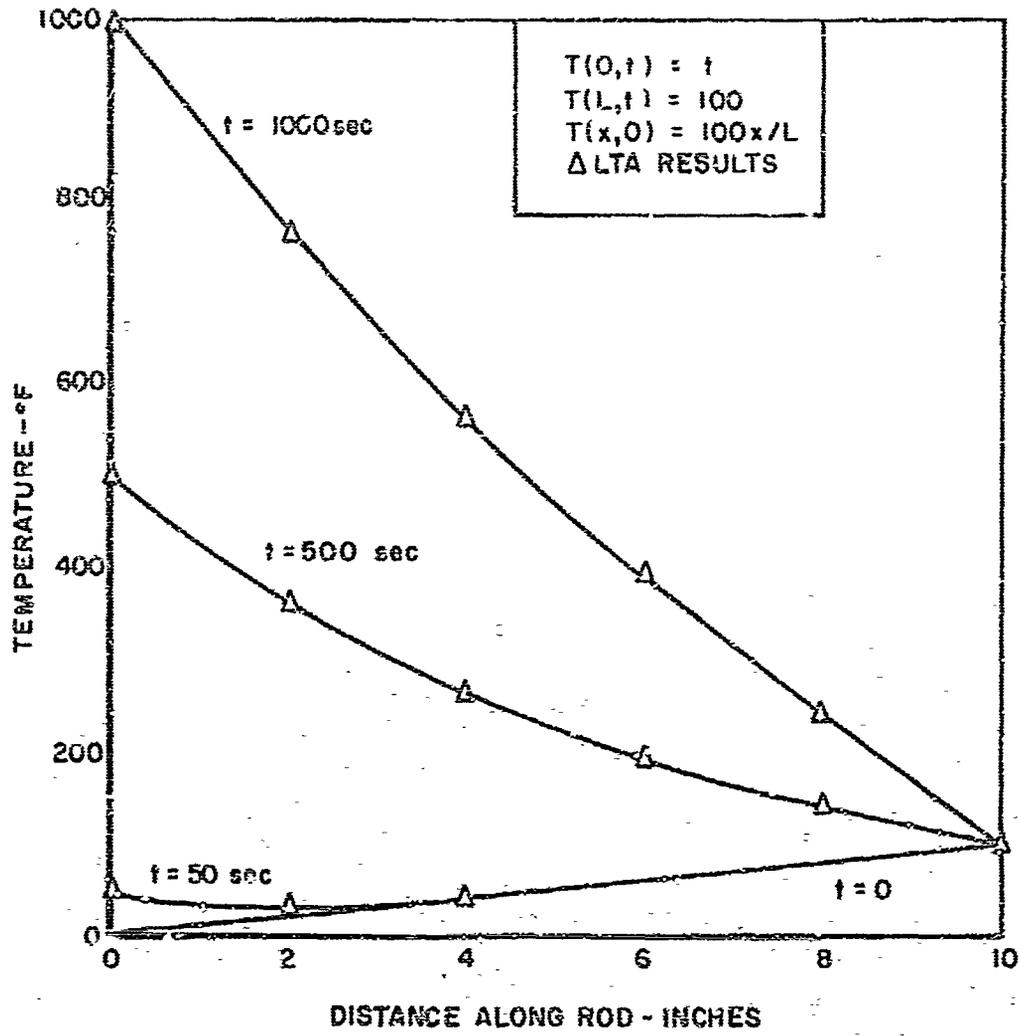


Figure 10. Temperature Profiles (Case 3)

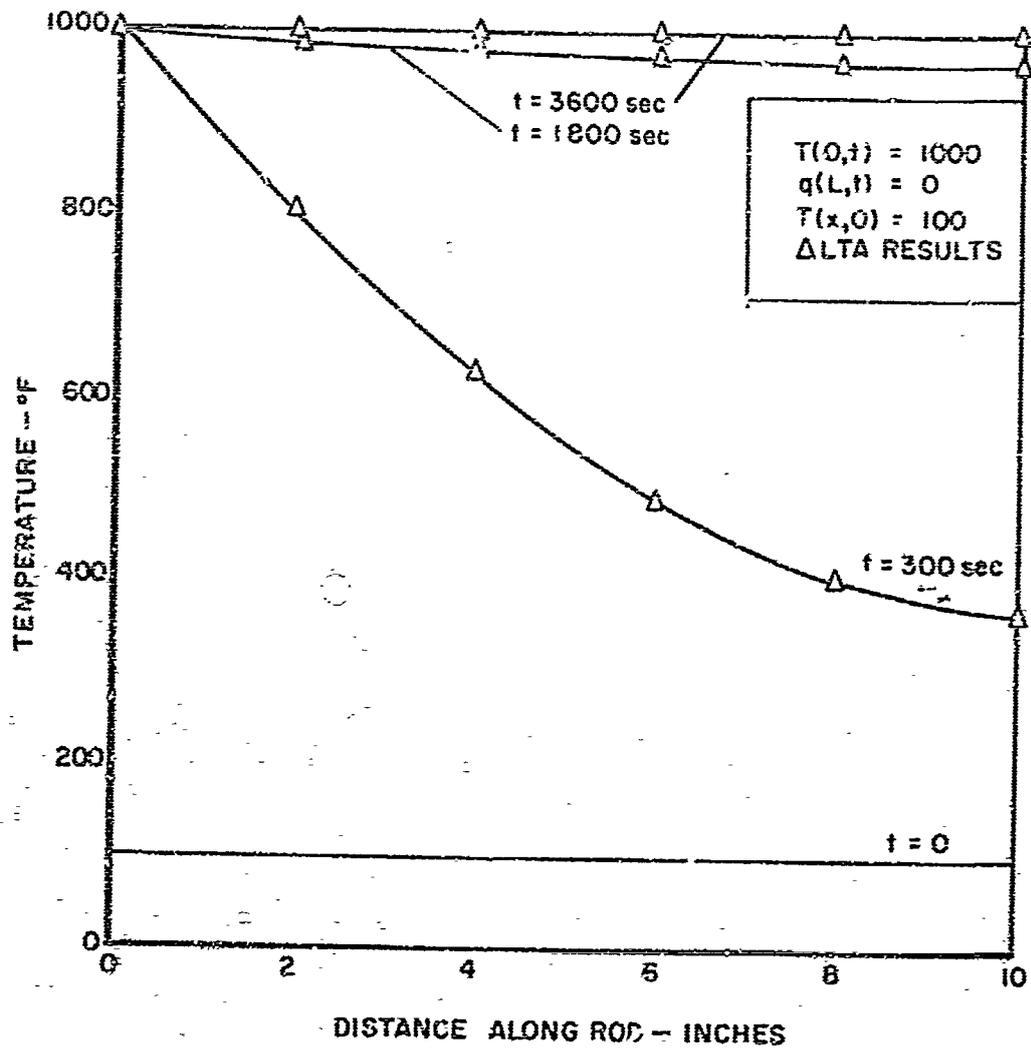


Figure II. Temperature Profiles (Case 4)

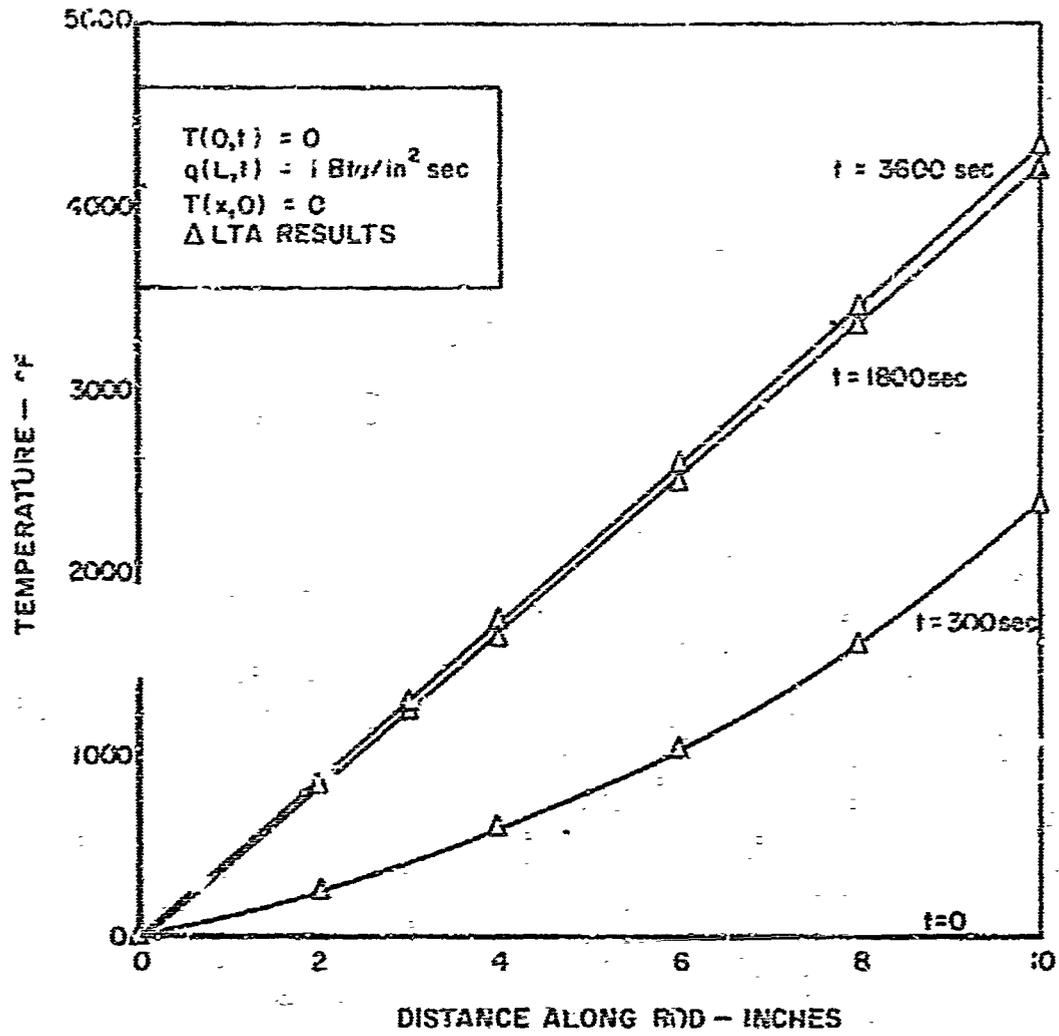


Figure 12. Temperature Profiles (Case 5)

Unclassified

Security Classification

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TRANSIENT ANALYSIS OF HEAT CONDUCTION THROUGH A SLAB BY INFINITE SERIES			
4. DESCRIPTIVE NOTES (Type of report and inclusive dates)			
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13. ABSTRACT			
<p>The exact solution to the problem of conduction of heat through a slab is developed. The solution, formulated in terms of an infinite series, allows arbitrary initial conditions and time-dependent boundary conditions. The solution is programmed in FORTRAN IV for the IBM 7094 II computer. Several check problems were solved and the results were compared with those obtained from a finite difference heat transfer program.</p>			

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KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Thermal Analysis Mathematical Formulation Digital Computer Analysis Arbitrary Boundary Conditions Infinite Series Computer Program One-Dimensional Transient Conduction FORTRAN						

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